Former private garages site at Princess Avenue Clitheroe

Proposed housing

Flood Risk Assessment

NGR SD 746 423

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1.0 Introduction

Four apartments are proposed for a former private garages site between 15 and 17 Princess Avenue, Clitheroe. This report covers the flood risk and surface water aspects of the proposal.

2.0 Executive summary

Four apartments are proposed for a former lockup garage site. The site is floodzone 2 on the Environment Agency floodrisk zone maps. Detailed hydraulic river modelling shows that risk levels are lower and the site is in practice floodzone 1. The proposal is suitable for the residential area, surface water discharges to the beck will reduce in terms of flow rates and volumes and flood risk to others will decrease. New hard area will be less than before and SR744 is complied with.

3.0 Existing site and river system.

The existing site is a block of former rented private garages with an access from Princess Avenue between house numbers 15 and 17. The site has been surveyed and has a level range of 76.86 to 77.3. There is a concrete slab yard area in front of the garages which slopes towards the stream and runoff from the overall hard area of approx 200m2 will flow straight into the stream. Chatburn Beck (Pimlico watercourse) flows through the site in open channel. The Beck flows under Princess Avenue in culvert and also flows into a culvert approx 40m downstream of the site. To the west of the site the gardens and private ground to Well Court slope away to a lower level

The upstream beck catchment has a catchment area of 1.61 km2. Annual rainfall is 1222mm, average bedslope DPSBAR is 40.3 m/km indicating a flattish catchment and SPRHOST is 30.24%. The catchment is thin with a length to width average ratio of 2.

4.0 Hydrology and river modelling

WinFAP3 software has been utilised to find similar catchments. A pooling group analysis was then carried out resulting in a Q100 flow of 4 m3/sec. This is approx 2.5 times the area and based on our own in house data from the analysis of over 200 small catchments is the sort of figure we would expect. To uprate the Q100 flow to Q1000 a growth factor of 1.7 has been used. Q100 + CC is 4.8 m3/sec and Q1000 is 6.8 m3/sec.

Cross section points have been selected on the site survey and cross section data input to Hec Ras 4.1.0 using survey levels. The river channel consists of vertical brick walls with a natural bed and 'n' values of 0.020 walls and 0.035 bed have been input. As can be seen on Google Earth the land to Well Court is lower and flow can spill over the channel wall towards Well Court. A lateral sideweir has been put into the model at the channel bend to simulate this.

The model has been run for Q100, Q100+ CC, and Q1000 flows. Cross sections 2 to 5 apply to the proposal and risk level results are as follows:-

Q100- flow 0.2m to 0.8m below the channel wall

Q100 + CC- flow 0.15m to 0.25m below the channel wall Q1000- flow level at wall top level to 0.35 below the channel wall

The results show that the site is floodzone 1 above the 1 in 1000 year risk level. We applied to the Environment Agency for risk levels for the beck and the 1 in 1000 year risk levels at the EA nodes 0421 and 0461 are 750mm above existing ground levels which is unlikely to occur in practice as sidespills will occur. We expect that the EA modelling will have cross sections with 'glass walls' at either side of the channel which produce artificially high risk levels.

5.0 Proposals and drainage

The proposals are for the demolition of the garages and the building of four apartments as one building. Drainage will be separate system with surface water draining to the beck and foul draining to Princess Avenue public sewer system via a submersible pumping station.

The guidelines for surface water runoff management for developments (2004 Gibbs paper) have been revised in Jan 2012 and are now contained in SR744 – 'preliminary rainfall runoff management for developments'. They allow comparison of proposals with the existing drainage performance of the site (principle 4) and on this basis surface water runoff rates and volumes will decrease as a result of the proposal and surface water attenuation will not be needed.

The beck is in open channel form between Princess Avenue and Well Court boundary where it goes into culvert. The culvert inlet is a blockage risk point and access is from Well Croft or 2 Causeway Croft rear garden. The beck channel inside the site is brick walls and access to the beck is at present from the access road to the existing garages and will continue to be so if the proposal is consented. The new apartments garden areas and the new building is shown partly within the 8m strip that the EA can ask to be kept clear, however the beck channel access is by climbing down into the channel from the access roadway and we would suggest that the proposal will not compromise maintenance access.

6.0 National Planning Policy Framework and Technical Guidance

The proposals are for housing, and are classed as 'more vulnerable' in Table 2, and are 'appropriate' in floodzone 1 as per Table 3.

All forms of flooding (PPS25 notation) are:-

C4 – rivers – see above

C5 – sea – no tidal influence

C6 – land – no undrained land slopes towards either site

C7 – groundwater – no springs or weep areas on site

C8 – sewers – no reported incidents of on-site sewer flooding

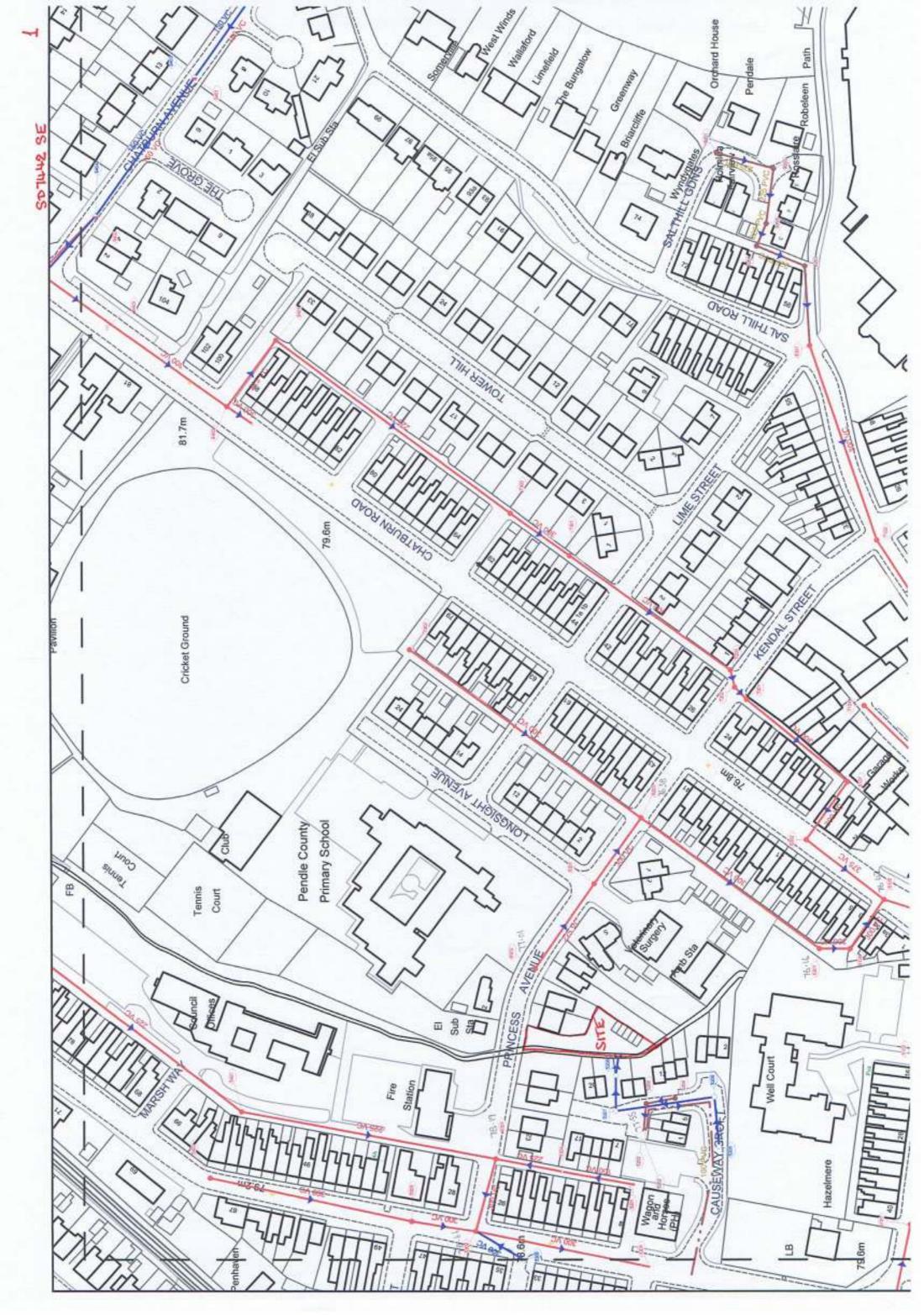
C9 – reservoirs, canals – none nearby

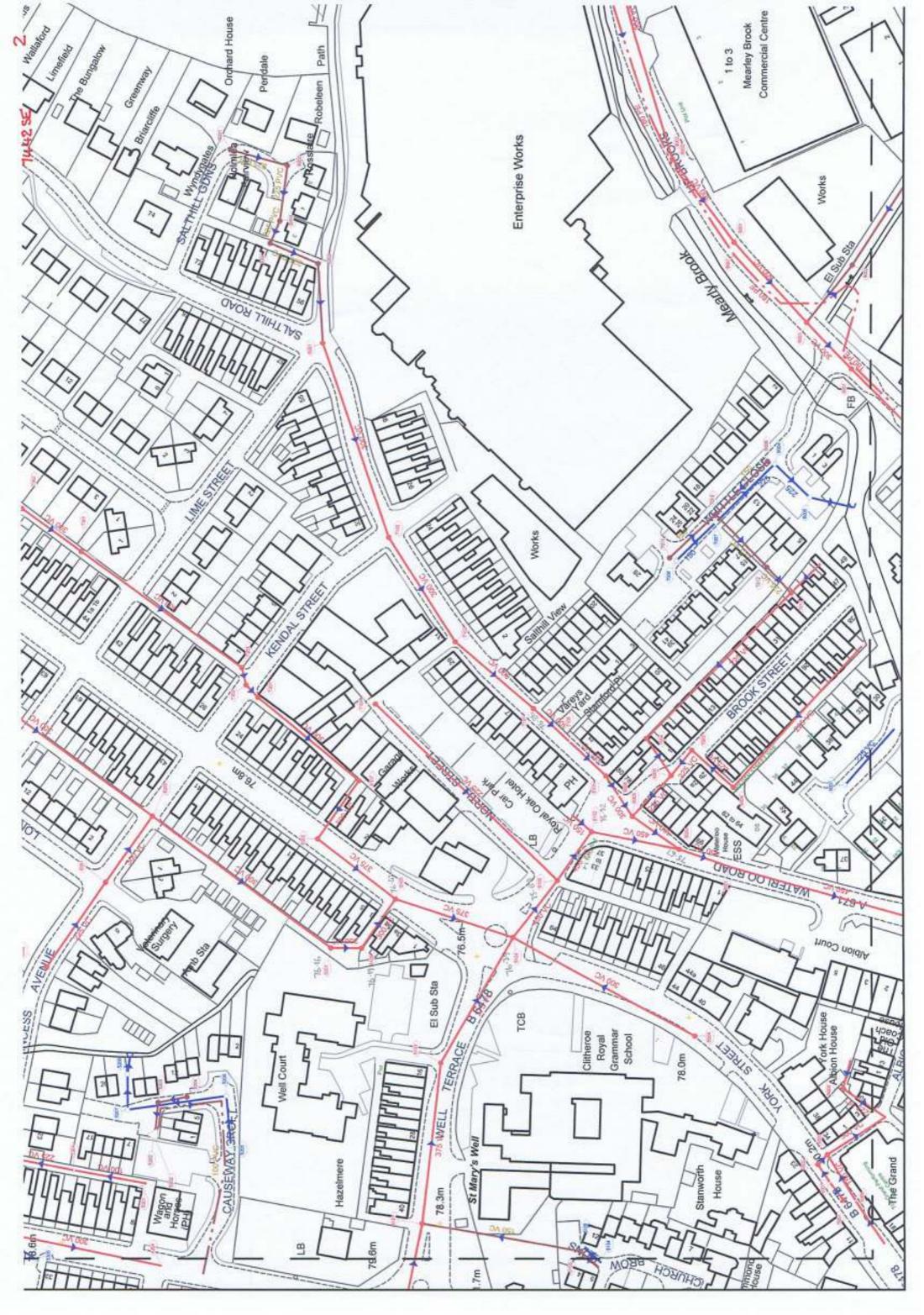
7.0 Attachments

Attachment	number	size
Site location and sewer	1 to 5	A3
records		
Site survey and river cross	6, 7	A3
section positions		
Proposals	8	A3
Environment Agency risk	9, 10	A3
level data		
Hec Ras outputs Q100,	11 to 19	A3
Q100+CC, Q1000		
FEH catchment plan	20	A3
FEH descriptors	21	A4
FEH rain data	22	A4

This report is an email report and A4 and A3 attachments are grouped for scanning and can be put in order by using the top RH corner lettering.

Email file list 130205fra01 130206attach1-A3 130206attach2-A3 130206attach3-A4

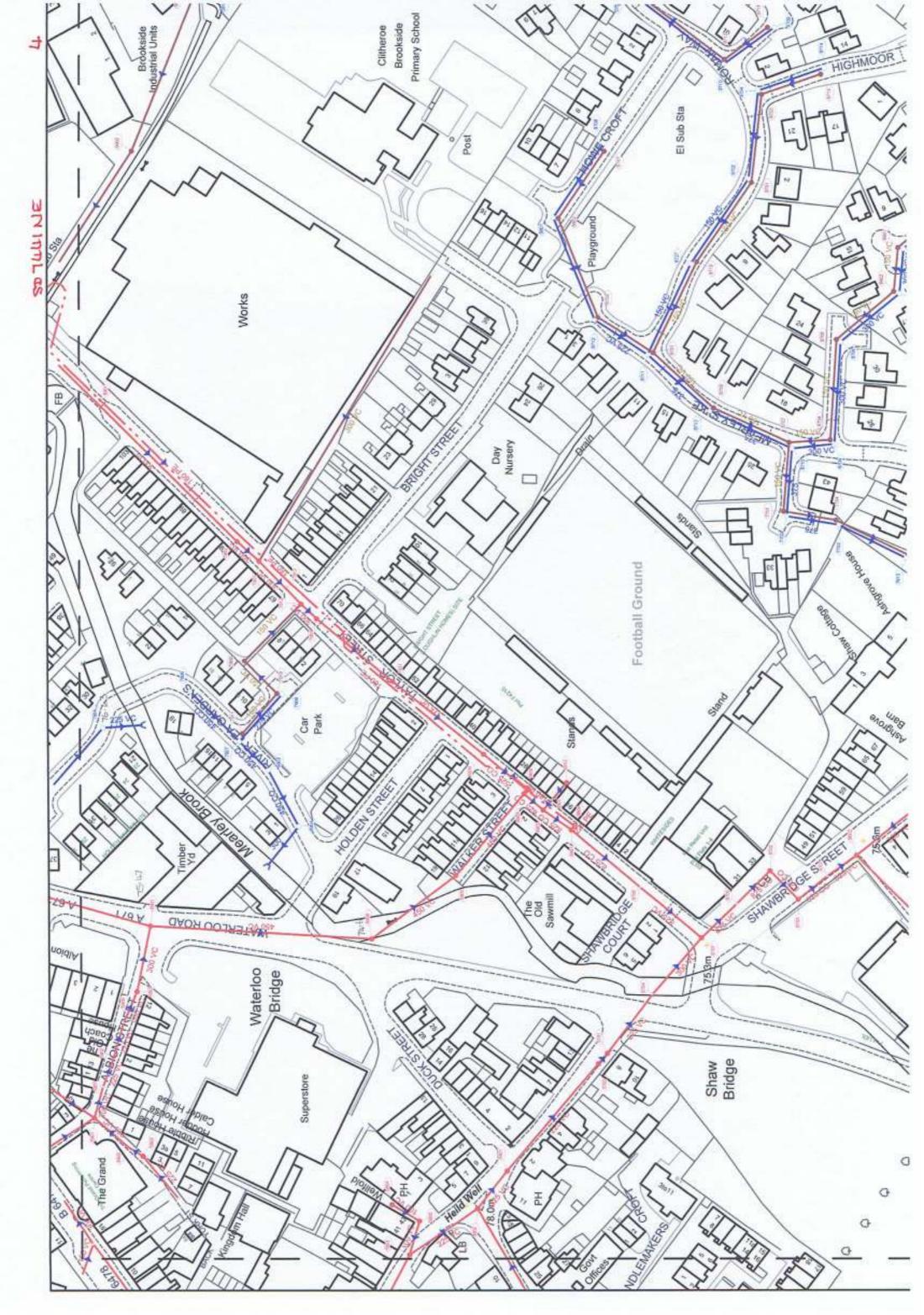




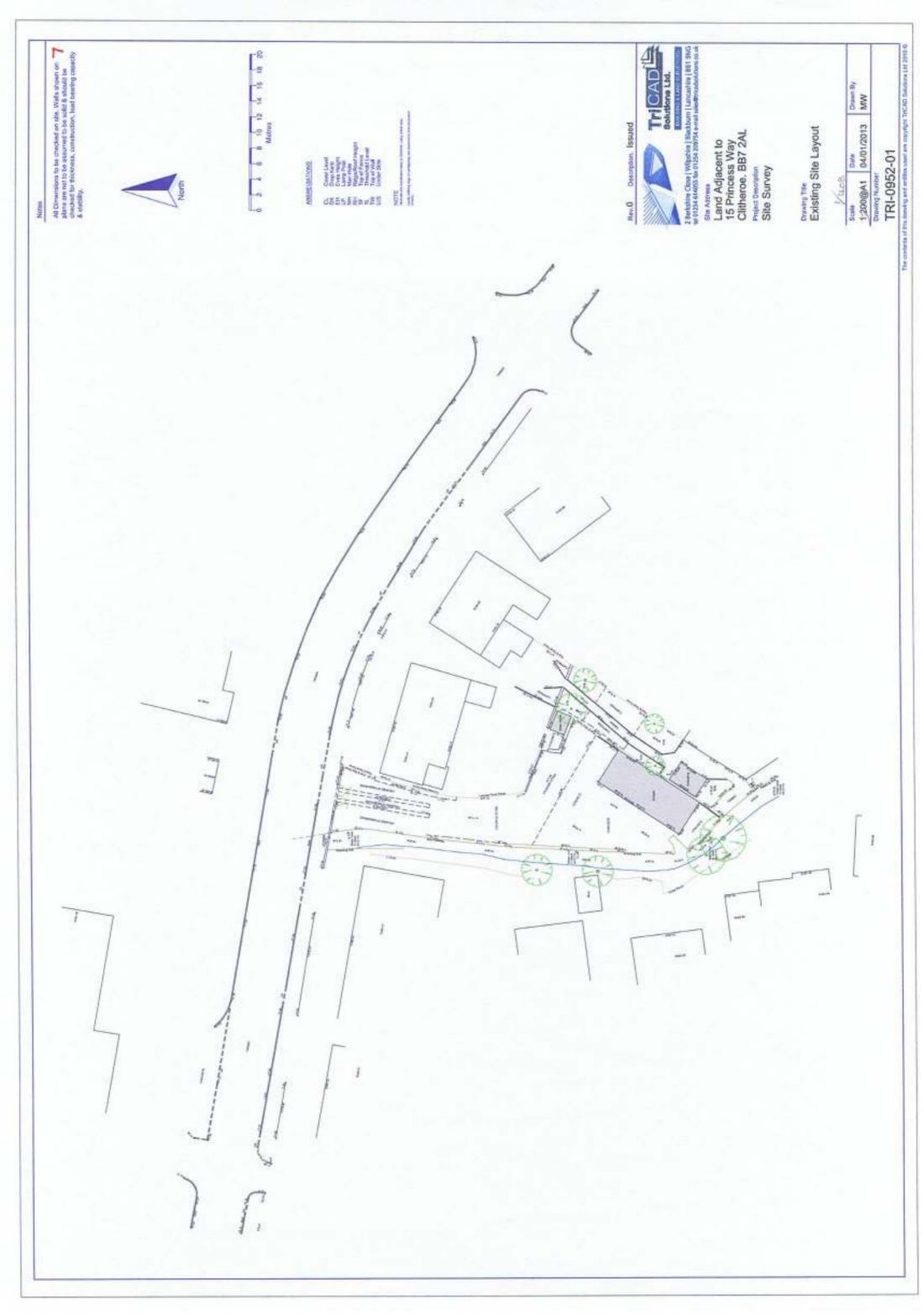
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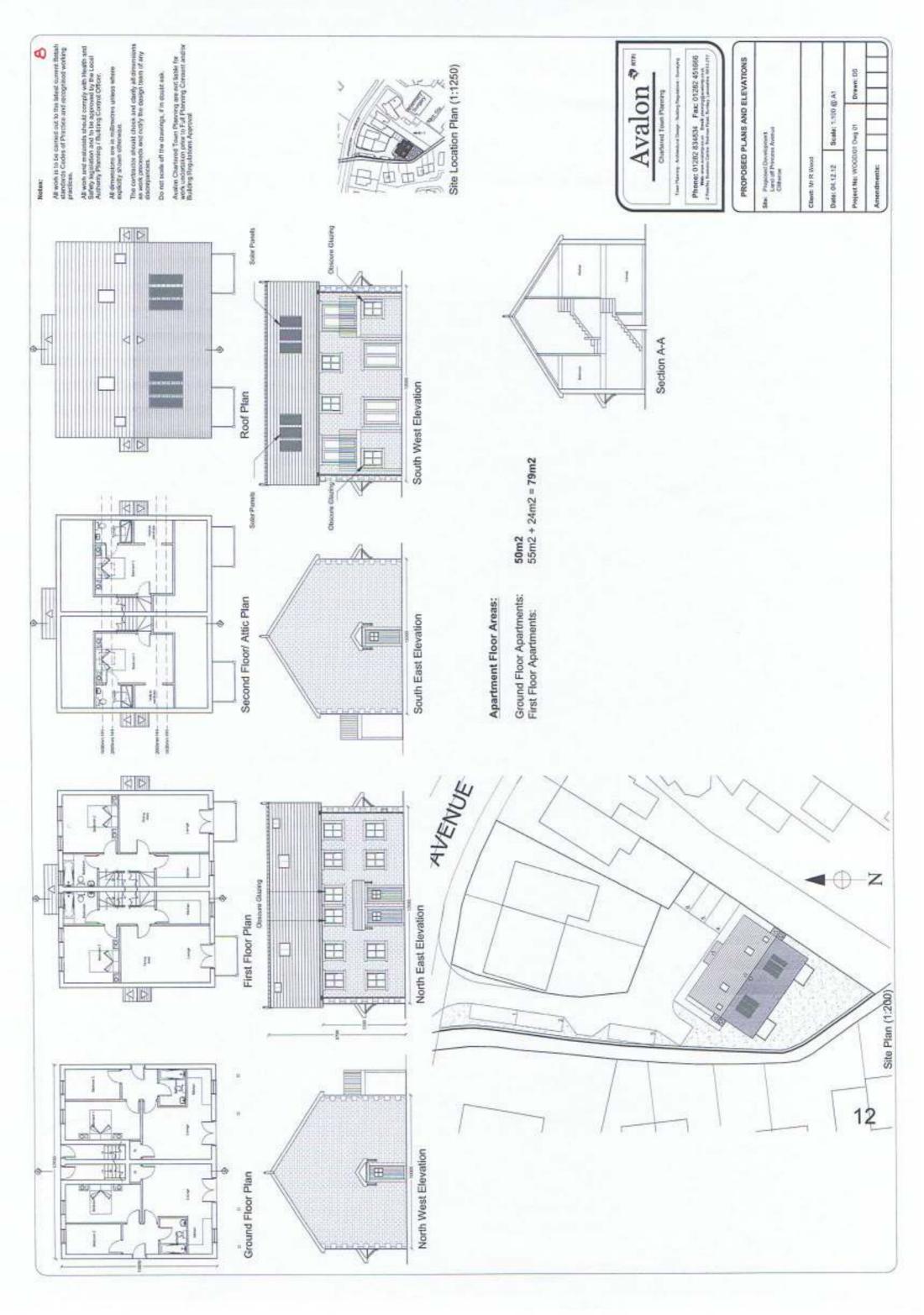
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36.0€ AC 0 83,33 150 0 8 84.84 18.33 AC. 120 a 6.0€ AC 120 48.88 20.35 21.85 DAG 11 23.09 DAG 0 325 7.97 \$8.04 DA. 0 300 Э 70,87 2006 75,52 AC. 0 300 26.37 W 0 2,17 1008 9 3 9096 300 99 AC. 0 ٦ 0 8403 12.18 AC 2 300 W 0 17.67 14,18 2009 25'44 AC 0 355 79,72 0 14,18 183 0 114.15 AC. 0 332 80,18 15.15 AC 0 200 d 58,77 2028 W 61,03 200 W 0 89,77 AC. 0 1028 112.66 0 100 180 € 94 H 7008 82.62 69 120 59'94 4 FIL 21,71 96 24,75 \$ 9008 19.03 25.42 300 2002 66.82 OA 300 2008 86 94 AC. 300 74.55 2 68.97 1008 208 412,06 300 76.21 3 11.11 220 28.58 77.23 0 300 PS.TT PSTT-AC. 90'94 9 48.97 96'9 30 DA. 300 90'94 0 97,97 7203 6.73 AC 300 0 **69'91** 7202 AC. 3 7201 AC 376 D 90'66 352 ۸¢ Z.04 192 AC 300 0 19.25 541 AC. 300 73.73 c \$6,08 352 AC 0 25,87 1013 13.84 332 7012 124 £ 1.97 65 24.77 190 76.37 W 4 7.87 1104 89 76.87 7.82 AC 338 W # 98'94 2010 S 6007 3 32.49 552 8 **L00**L 35.35 W 8'94 21,76 091 W 8 99794 9002 0 TA.TP AC 338 w 1004 12.86 ۸C 552 0 4.91 552 0 98,87 AC 525 1007 69.04 338 10.17 8.16 AC 300 AC 300 28.88 38,44 AC 212 M 0 12,01 AC 200 W 1029 0 29'6 AC 420 8019 £ 9 28,11 AC. 200 4019 39"9" W 0 14.87 991 23.61 141 AC 300 74.16 0 61,87 9019 10.80 NC SIC 86,67 0 75.87 38.85 AC 059 73,73 0 86.37 AC. 059 0 23,46 NC 097 0 16.8 AC 946 W 0 29:21 84 NC 552 74.89 W S 76.25 2009 47.6 NC 300 23.67 D 0 9009 3A 525 0 9009 55.26 W 166 21.64 AC 0 552 0 8.87 \$009 13.89 W 0 121 5533 AC 0 300 73,49 8.87 0000 w 0 20.5 ΛC 5 095 62.27 18.87 2000 W 16.38 ΛC 3 190 ٦ 3 0004 27.0B 188 ΛC 300 81.17 W 0 47,67 2019 101.21 202 550 42,77 0 265 26.49 1-005 253 26.33 2312 69:39 0 99.87 230 29,84 AC. 200 **CT.8T** W 0 1009 8 L 225 W 14.03 7058 29 W S 9029 W S 9029 99'61 bAC 100 W P029 89,11 4 12.93 DAG 100 W 2203 4 104,46 C bAC 400 5202 77.65 d 4 284 28.36 AC 16.95 100 7 0 2504 S 2300 d 63.34 S 62.83 43 ΛC 3 4 61.78 143 ΛC 375 o £8.87 2015 ۸c 375 W 0 4.87 1015 21.21 120 D 0 8009 25,8 NC 225 Z-67 D 0 2009 20.05 NC 225 M 3 9009 12.23 NC 225 9 0 5009 60.18 C AC 300 1009 э Tr.08 5008 80.7S 45 C AC 00E E6.87 M 86.8 5 69.8 21 C AC C W 19'85 460



0916		5	F							752			F	м		150	c	vc		6.15	SOTUMNE
5501	74.18	C	м	70,39	900	С	VC		27.55	752			F	M		150	c	VC		3.65	
5502	74.62	C	м		225	c	VC		22.43	760			s	F							
5503 5504	75.19	C	M	73,62	225	c	VC VC		25.06 18.44	760 760		7.35	C	M	79.52	300	c	VC	21	32.17	
5505		C	G		225	c	VC		34.25	760		-35	F	M	74.9	300		**	41	22.51	
5506		C	L		225	c	vc		19.52	760			F	M						25,6	
5507	75.9	C	М	73.62	225	С	VC	142		760			F	M		300		VC		7.8	
5508 5509		C	G		225 525	С	vc vc		45.17 28.26	760 760			F	M		300		VC		25.04	
5601	75.46	c	M	70.88	900	c	VC	214		760			F	M		300		VC		9.63	
5701	75.16	C	M	72.63	225	Ç	VC	68	29.4	760			c	M		300	c	vc		26,73	
5702	75.14	C	М		225	С	VC		5.32	761			S	M						25.74	
5801	77.58	C	M	74.99	225	C	VC		55.57	761			5	M						11.33	
5802 5803	78.16 78.48	c	M	76.89	225	c	VC	10 204	18.75	761: 761:			5	M						8.22 22.35	
5804	1000	C	M	11700	100	c	vc	204	12.52	770			F	M						20.8	
5805		C	M		100	c	VC		14.34	770			s	M		375	C			20.64	
5901	77.62	C	M	75.3	300	C	VC	21	12.82	770			5	M						29.4	
5902 5903	78.27	C		74.06 76.1	225	c	VC	82	13.9 7.02	770-			F	M	90.49	275		146	220	32.69	
5904	rowr	c	M G	79.1	225	c	vc vc		21.66	780 790		1.93 5.37	C	M	72.43	375	c	VC	239	45.47 23.51	
5905		c	J		225	c	VC		17.28	790		5.66	c	M	73.26	300	c	vc	40	11,49	
5906		c	G		300	c	vc		20.49	790			c	M	72.69	376	c	VC	160	38.42	
5907		C	q	74.68	225	c	vc	21	12.86	790		1.63	S	м	74.53	225	c	VC		15.27	
5908 6501	81.08	C	M	73.89 78.98	300	c	vc vc	78 47	13.27	790		22	5	F.	74.58	450		nn	400	92.54	
6502	79.97	C	M	77.88	300	C	VC	44	43.1	790		.24	5	M	74.58	450 450	c	co	109	27,31 15.92	
6503	79.02	c	м	76.89	300	c	VC	27	51.61	790		5.86	5	м	74.57	225	c	VC	104		
6504		c	G		225	c	VC		33.21	790		(5.50)	F	м		150	c	VC	12000	31.48	
6505		C	J							791		5.85	F	M	74.17	150	c	VC		18.03	
6506 6507		C F	J		150		Wes		2.05	791		1.2	F	M	74.77	150	C	VC	36	20.79 B 42	
6508		F	3 D		150	c	VC VC		2.65	791: 791:			C	H	74,48	180	c	VC PE	162	5.42 149.26	
6509		s	D		150	c	VÇ		3.18	850		2.8	C	M	88.7	300	c	VC	21	64.88	
6510		s	3		150	C	VC		3.26	850	88	8.19	c	M	85.56	300	c	vc	30	26.05	
6511		F	D		150	c	VC		3.47	850		5.82	C	M	84.62	300	c	VC	16	79.62	
6512 6513		5	D		150	C	VC		2.26	850 850			S	M			C			28.97	
6514		F	1							860			F	M		150	c	VC		17.27	
6515		c	M		100	C	VC		2.96	860			F	M		150	c	VC		29,48	
6516		C	M		100	C	VC		21.81	860			F	M		150	c			57.98	
6517		C	M		100	C	VC		12.15	860			F	M						15.52	
6518 6519		C	M		100	С	VC		7.79	850 860			S	M		300	С	VC		9.58 17.63	
6520		c	3							860			S	M		300	c	VC		30.04	
6601	76.19	c	M	73.35	300	С	VC	22	36.54	860			s	M		150	c	VC		58.67	
5602	75.57	c	M	71.27	900	С	VC	263		560			s	м						16.22	
6603	75.96	C	M	73.33	300	C	VC		26.57	861			S	М						29.33	
6701 6702	75.09	C	M	71.63	825 825	C	CO		19.17 15.73	861 870			F	M		150	С	vc		16.1 32.15	
6703		c	M		825	c	co		14.6	870			F	M						25.71	
6704		c	Q	72.2	300	С	VC	70	29.42	870			F	M		150	С	VC		32,46	
6705		C	Q	33.83	825	С	CO		18.54	870			F	M		150	С	VC		16.16	
6706		C	0	71.39	825	c	VC	-120		870			F	M		150	c	VC VC		39.55	
6707 6801	74.77	C	M	33.32 71.27	825 825	c	co		14.1 35.05	870 870			S	M		150	c	VC		40.25 27.16	
4802	74.73	C	M	71.95	825	c	co		13.52	870			s	M		300	c	VC		16.7	
6803	74.73	c	M	71,99	825	С	co		9,87	871	0		s	M		375	c			26.71	
6804	74,79	C	M	72,22	525	c	CO		22.1	871			8	M		375	c	12.5		32.89	
6805	75	0	M	72.37	450	c	VC		41.92	871			8	M		225	c	VC		24.89	
6806 6807	74.6	C	M	72.7	450 150	c	vc co		41.35 5.49	871 871			S	M		375 150	c	vc		35.23 39.84	
6808	74.75	c	J	73.75	225	c	PE		1.99	872			s	M		150	c	vc		39.85	
6809	74.7	c	м	71.96	525	c	CO		1.78	880			F	G		300	C	VC		131.73	
6810	74.61	C	М	73.1	300	С	VC		8.74	890		SHEET.	c	н	75.17	180	С	PE	151		
6901	75.47	C	М	72.87	450	c	VC		86.8	950		3.76	C	M	90.29	300	c	VC	21	33.92	
6902 6903	75.6 76.05	S	M	73,69	300 450	c	CO		26.3 25.09	960			F	M						59.06 36.28	
6904	10.05	8	M	74.18	300	c		201	19.23	960			F	M		150	c	VC		33.94	
6905		s	F		(0.00)	110			WHE.	960			F	M		3557	11.11	3.2		24.04	
7500		F	J							960			F	M						24.9	
7501		F	D		150	С	VC		4.68	960			F	M						31.75	
7502		S	D		150	C	VC		4.75	960			5	M						27.13 36.32	
7503 7504		5	D		150	c	vc		19,8	960			5	M						58.68	
7505		s	D		150	c	VC		25.89	961			5	м						33.89	
7506		F	D		150	c	VC		26.31	961			8	м						25.63	
7507		S	D		150	c	VC		11.14	961			8	м						32.72	
7508		F	D		150	c	vc		11.34	961			5	M		150		vc		17.65 37.65	
7509 7510		S F	D		150	c			13.89	970			F S	M		150 150	c	VC		40.18	
7511		S	D		150	c	VC		12.26	970			F	м		63500	- 22	0.00		34.59	
7512		p	D		150	c	vc		12.37	970			s	M						34.5	
7513		s	P		150	С	VC		58.66	970			F	м						31.79	
7514		F	D		150	c			59.25	970			S	М						35.26	
7515 7516		S	M		100	c	VC		26.73 17.97	970			S	M						24.26 52.62	
7517		F	D		150	c	VO		18.21	971			F	M						20.98	
7518		s	D		150	c			15.86	971			F	86						52,41	
7519		F	D		150	С	VC		16.47	971	3		F	M						24,44	
7520		S	D		150	c			27.52	971			S	M						27.33	
7521 7522		F	D		150	c	VO		27.61 14.47	980			S F	M						43.44	
1522		S	D		150	C	VC		14.47	98	4		100	191						141.29	





Princess Avenue, Clitheroe Flood Map (NTH6802S)

Junction

4 LE

B

SD 74600 42300 National Grid Reference:



North West Region - North Area

Tel: 03708 506 506 www.environment-agency.gov.u/ Walton Summil, Bamber Bridge, Preston, PR5 8BX Lutra House, Dodd Way, Off Seedlee Road,

Produced by Flood Risk Mapping

6 February 2013 Map produced on:

Legend

Modelled Flood Group

Node Point

EA01210PIML01 0471A

Ground

Main River

Flood Zone 3

Flood Zone 2

EA01210PIML01 0392

88543

WORB

Y.S.S.7

EA01210PIML01 0421

USEV

L01_0461

EA01210PIM

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ALLEYS

EA01210PIML01_0471B

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will use reasonable care to ensure an accurate copy of the data. The accompanying disclaimer should be used in will always be accurate, up to date or valid but the Agency The datasets used in this plan may not have been audited. The Agency cannot ensure that the data in its possession conjunction with this plan.

Metres

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Flood Zone 3; Shows the area that could be affected by flooding from rivers or the sea, if there were no defences. This area could be flooded:

from the sea by a flood that has a 0.5% (1 in 200) chance or greater of happening each year.

(F)

MEM

AV G

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WAY

RA

Flood Zone 2: Shows the additional extent of an extreme flood from rivers or the sea, if there were no defences. These outlying areas are likely to be affected by a major flood, that has up to a 0.1% (1 in 1000) chance of occurring each year. or from a river by a flood that has a 1% (1 in 100) chance or greater of happening each year.





Undefended Level (mAOD)and Flow (m3/sec) data for Citheroe

		15	10	0	25	2	ĬŇ	20	7	20	100	0	200	0	1000	00
	Level	Flow														
EA01210PIML01 0392	75.45	1.98	75.5	2.27	75.58	2.77	75.67	3.35	75.73	3.77	75.77	4.06	76.03	4.8	77.74	7.66
EA01210PIML01_0421	75.8	1.98	75.85	2.28	75.93	2.77	76.02	3.36	76.07	3.78	76.11	4.07	76.2	4.82	77.74	7.77
EA01210PIML01_0461	76.41	1.98	76.47	2.28	76.56	2.78	76.66	3.36	76.72	3.78	76.76	4.08	76.86	4.84	77.75	7.82
EA01210PIML01 0471A	76.52	1.98	76.59	2.28	76.72	2.78	76.87	3.37	76.98	3.79	77.05	4.08	77.23	4.84	77.85	7.82
EA01210PIML01_0471B	76.46	1.98	76.53	2.28	76.63	2.78	76.74	3.37	76.81	3.79	76.85	4.08	76.96	4.84	77.74	7.82

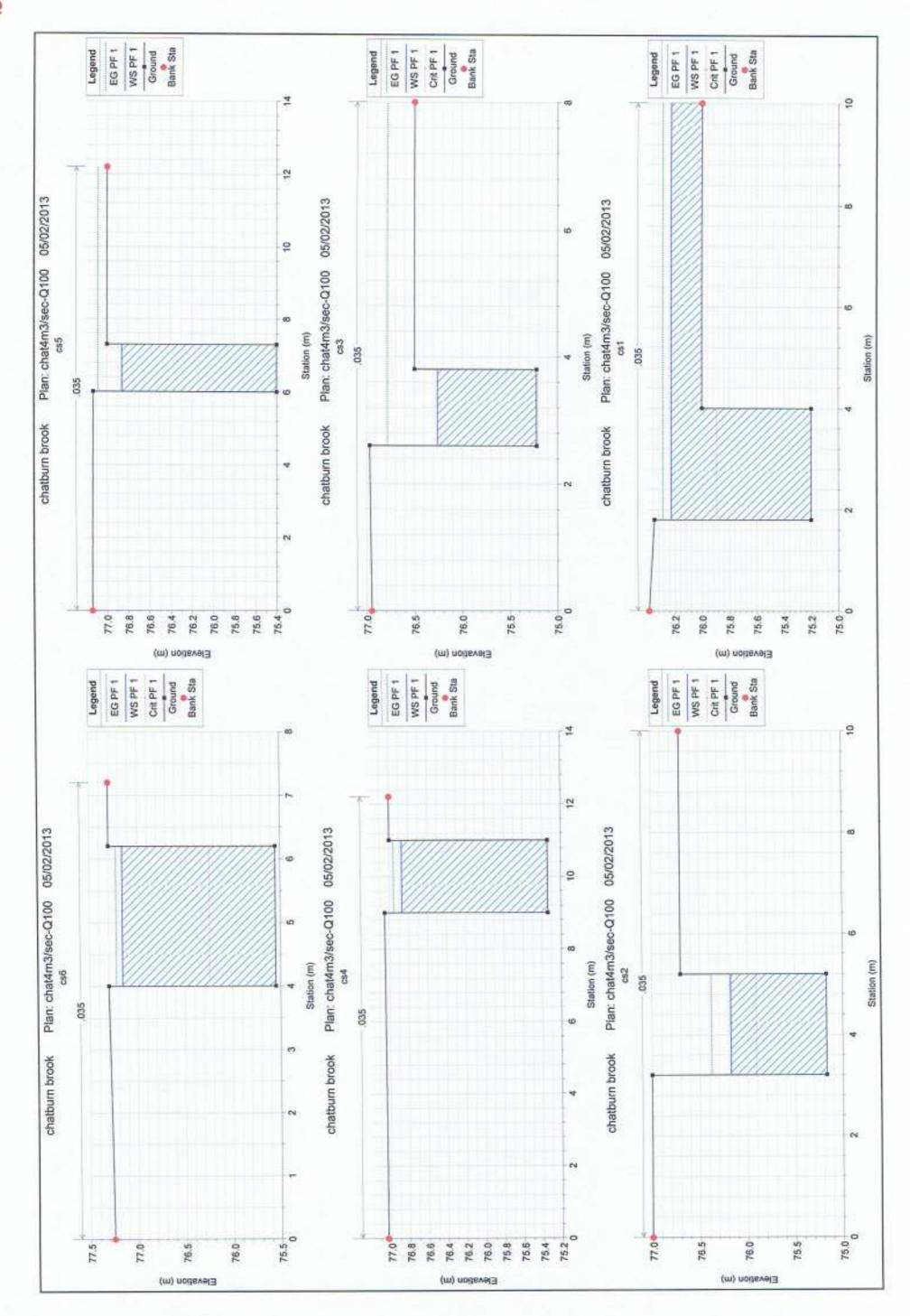
Data taken from Mearley SFRM Study

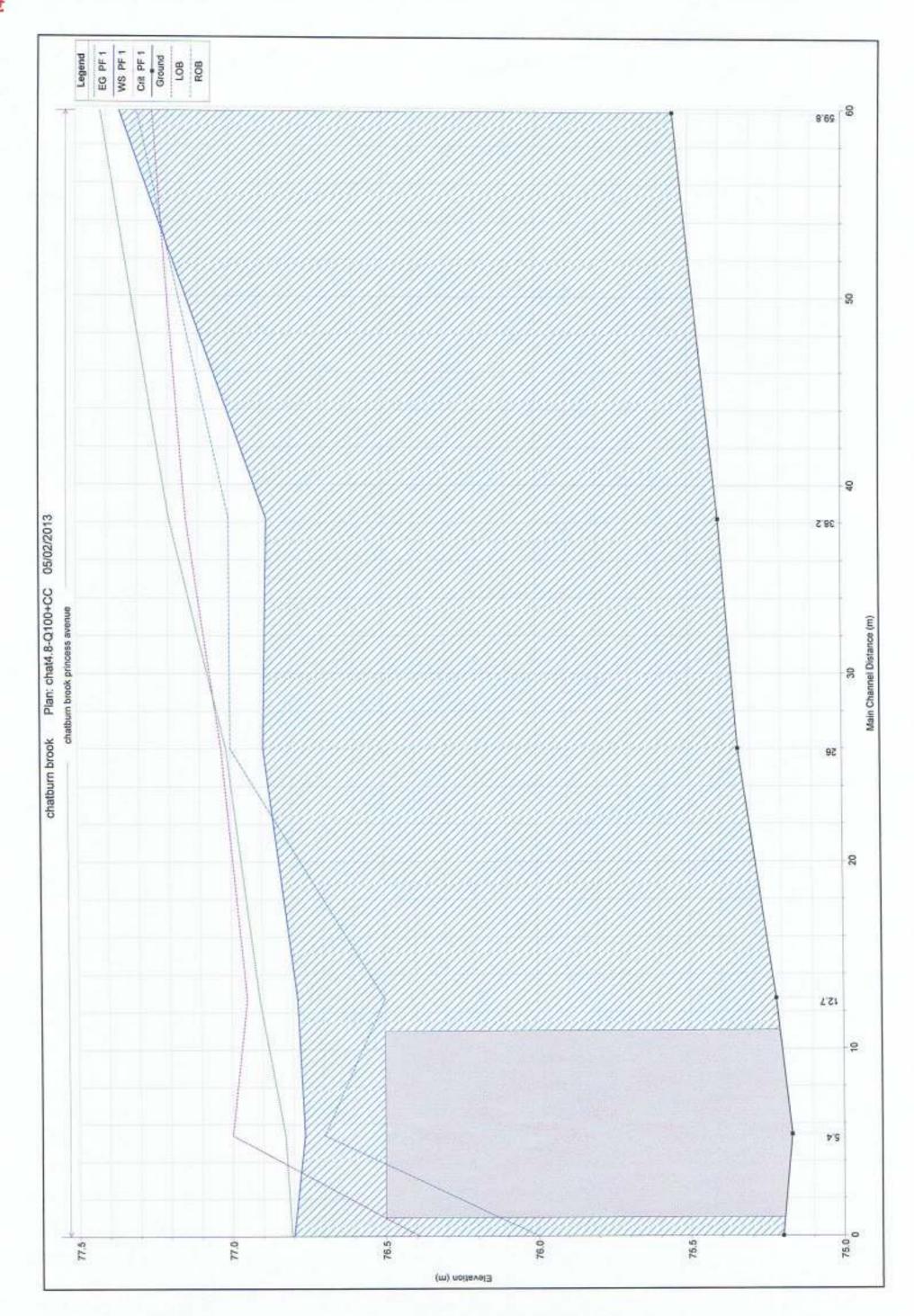
Defended Level (mAOD) and Flow (m3/sec) data for Clitheroe

	1	10	S	20	7	75	10	100
	100	Flow	Level	Flow	Level	Flow	Level	Flow
A01210PIML01 0392	75.5	0	75.67	0	75.73	3.76	75.77	0
A01210PIML01 0421	75.85	0	76.02	0	76,07	3.78	76.11	0
A01210PIML01 0461	76.47	0	76.66	0	76.72	3.78	76.76	0
A01210PIML01 0471A	76.59	0	76.87	0	76.98	3.78	77.05	0
A01210PIML01 0471B	76.53	0	76.74	0	76.81	3.78	76.85	0

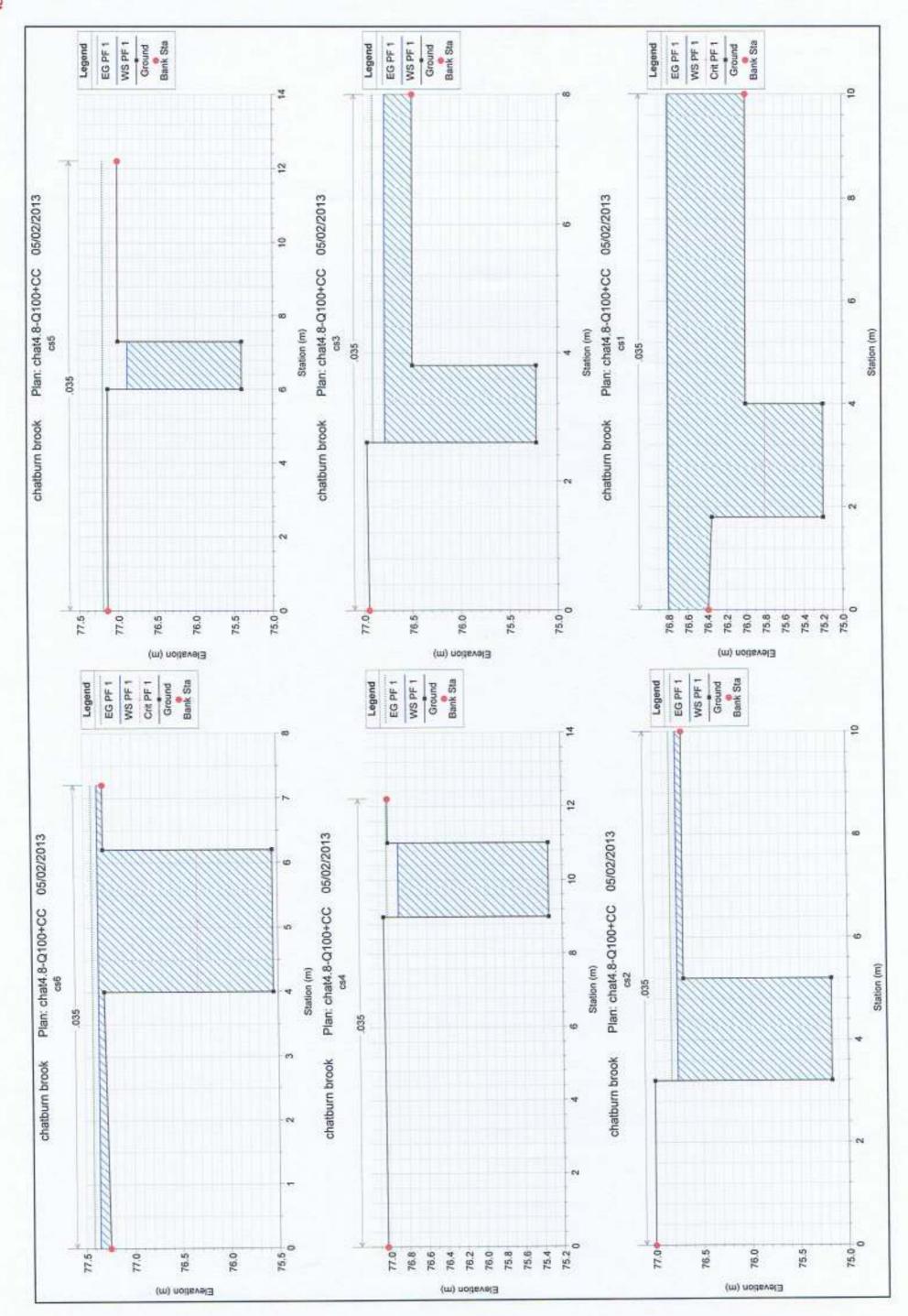
Data taken from Mearley SFRM Study

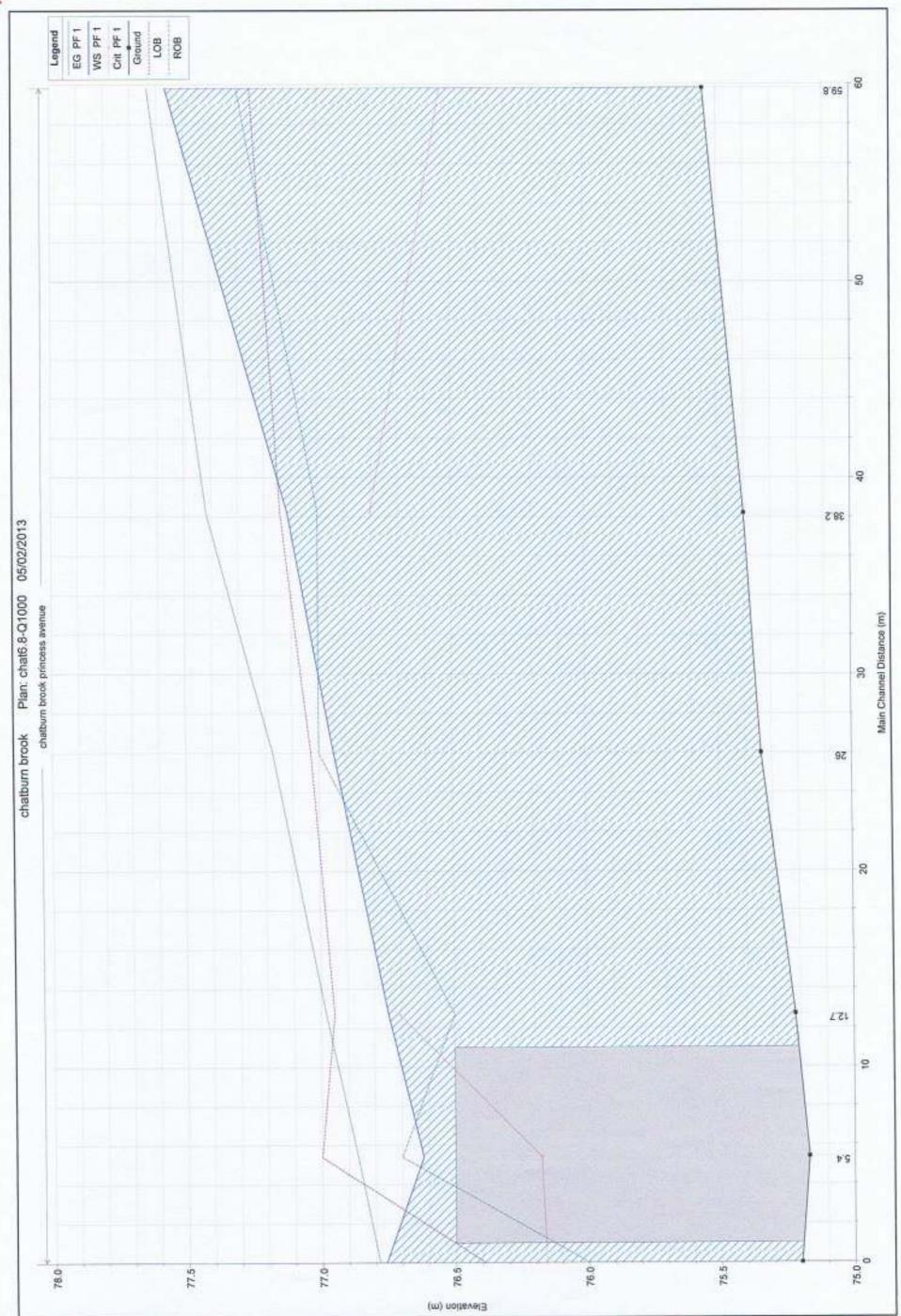
Reach	River Sta	Profile	Q Total	Min Ch El	W.S. Elev	Crit W.S.	E.G. Elev	E.G. Slope	-	Flow Area	Top Width	Fronde # Chl
			(m3/s)	(H)	(w)	(m)	(m)	(m/m)	(m/s)	(m2)	(iii)	
nincess avenue	59.8	PF1	4.00		77.16	76.24	77.22			3.53	2.20	0.29
nincets avenue	38.2	PF 1	4.00	75.40	76.85		77.09			1.90	1,30	0.56
	26	PF 1	4.00	75,34	78.87		76.96				2.00	0.34
rincess avenue	12.7	PF 1	4.00	75.22	76.26	76.26	76.78		3.21	1.25	1.20	1.00
orincess avenue	5.4	PF 1	4.00	75.17	78.17	75.91	76.38				2.00	0.64
princess avenue	0	PF 1	4,00	75.20	76.23	75.89	76.29				8.20	0.53



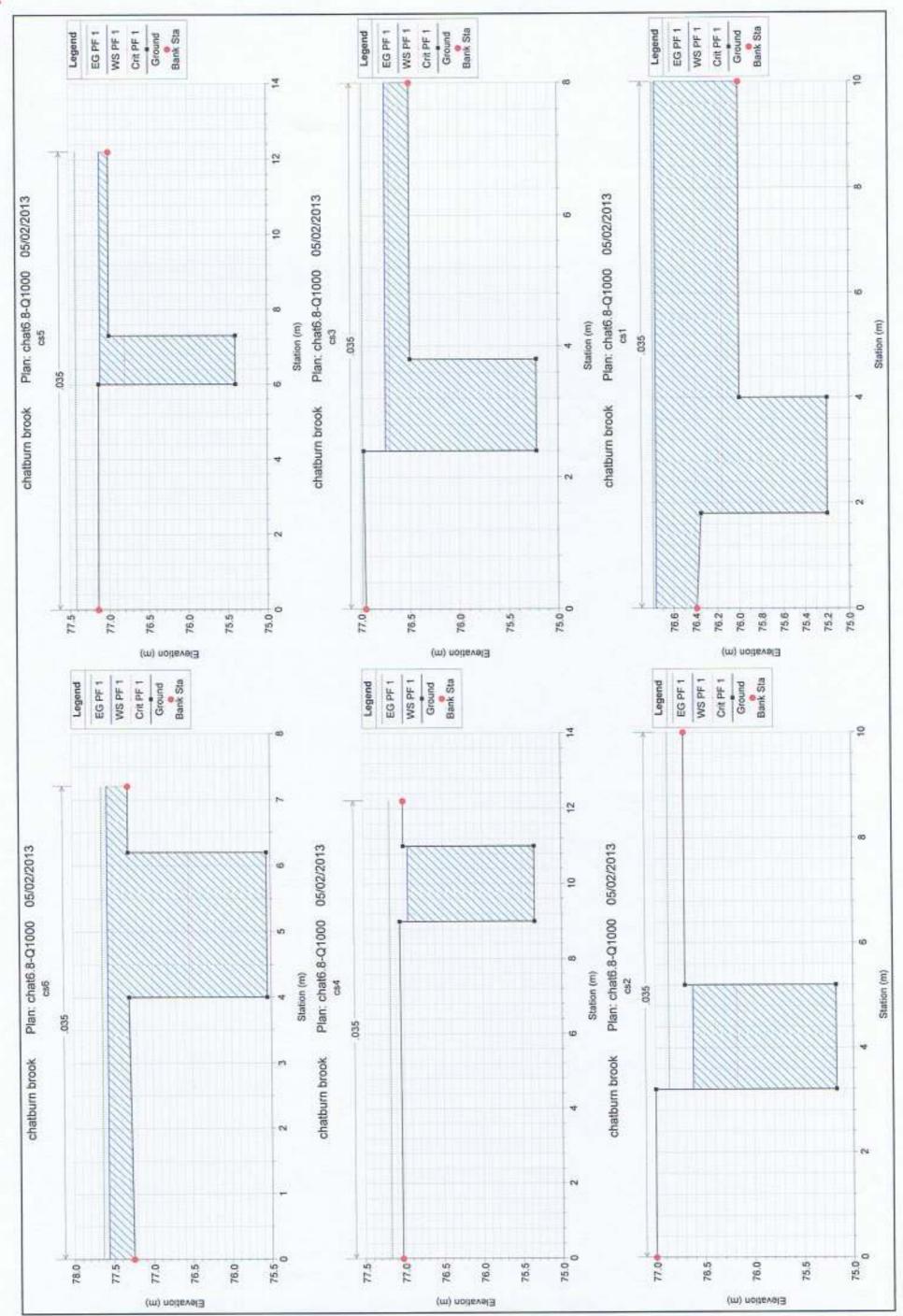


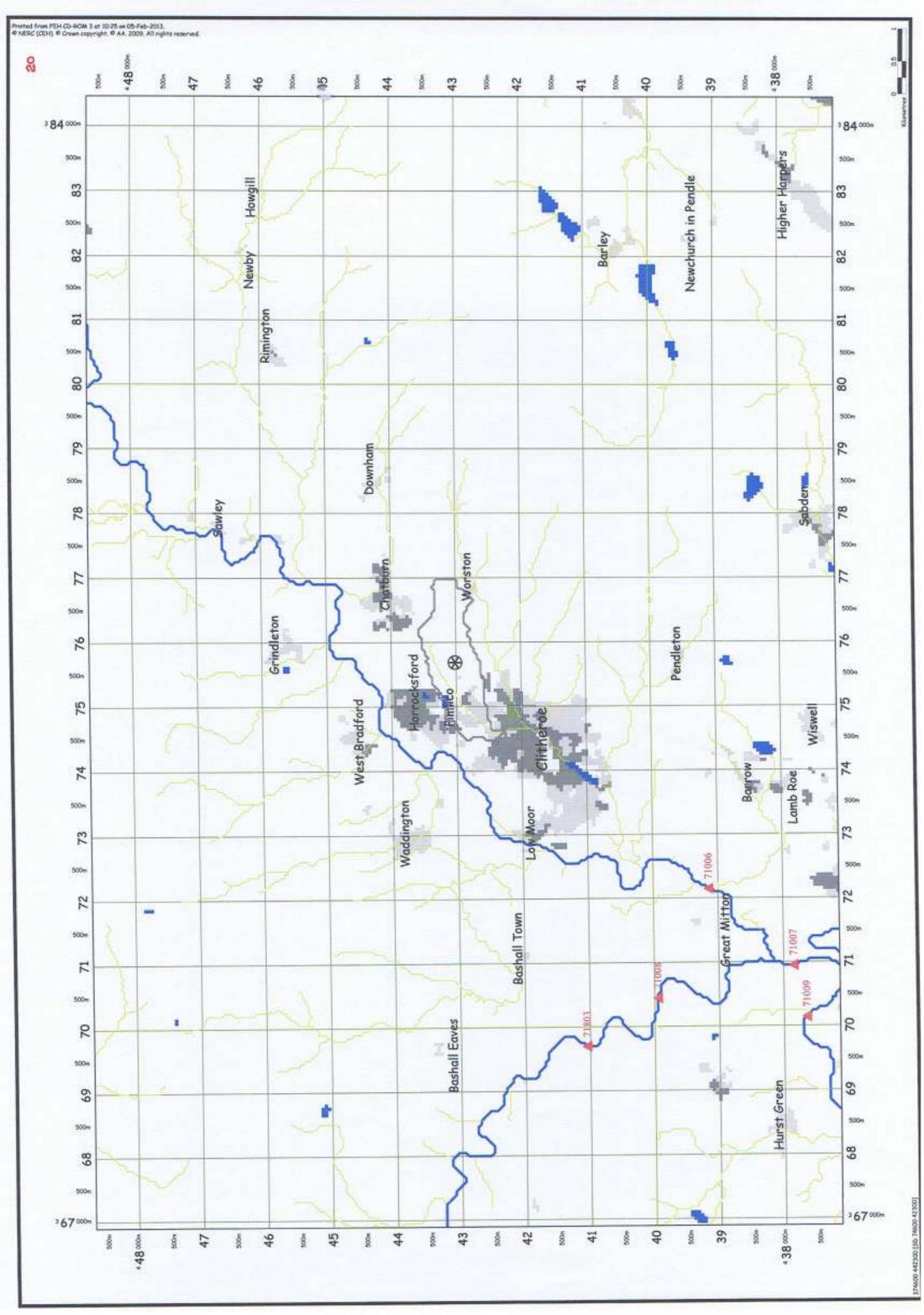
Reach River Sta Profile OT folal Min Ch El W.S. Elev Cal. Elev E.G. Slope Vel Chril Plow Area 1 pp VMIOR Fronce Month Profile OT 20 (m3/s) <	4 100 100 100	CO LINE COLUMN		The second second		The second division in which the second			ľ	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1174	War and Market Like	The state of the last
59.8 PF 1 4.80 75.55 77.36 76.33 77.42 0.005001 1.10 4.36 7.20 38.2 PF 1 4.80 75.40 76.89 77.20 0.022100 2.50 1.92 1.30 26 PF 1 4.80 75.34 76.89 77.01 0.005682 1.55 3.10 2.00 127 PF 1 4.80 75.22 76.79 76.91 0.011611 1.56 3.08 5.40 11 Lat Struct 75.17 76.76 76.83 0.006302 1.13 3.49 6.80 5.4 PF 1 3.94 75.17 76.80 76.81 0.000253 0.35 9.10 10.00	Reach	River Sta	Profile	O Total	Min Ch El	W.S. Elev	Crit W.S.		-	VelChul	Flow Area	Top Width	Propose # Call
59.8 PF 1 4.80 75.55 77.36 76.33 77.42 0.0055001 1.10 4.36 7.20 38.2 PF 1 4.80 75.40 76.89 77.20 0.022100 2.50 1.92 1.30 26 PF 1 4.80 75.34 76.89 77.01 0.005682 1.55 3.10 2.00 127 PF 1 4.80 75.22 76.79 76.91 0.011611 1.56 3.08 5.40 11 Lat Struct 75.17 76.76 76.83 0.006302 1.13 3.49 6.80 5.4 PF 1 3.24 75.20 76.80 76.81 0.000253 0.35 9.10 10.00	and the same			(m34c)	(m)	(m)	(m)			(m/s)	٤		
59.8 PFT 4.80 75.40 76.89 77.20 0.022100 2.50 1.92 1.30 26 PFT 4.80 75.34 76.89 77.01 0.005682 1.55 3.10 2.00 127 PFT 4.80 75.22 76.79 76.91 0.011611 1.56 3.08 5.40 11 Lat Struct 75.77 76.83 0.006302 1.13 3.49 6.80 5.4 PFT 3.24 75.17 76.80 76.81 0.000253 0.35 9.10 10.00		-		100	76.66	1	78.33	1		1.10			0.45
38.2 PF 1 4.80 75.40 76.88 77.20 0.022100 2.50 1.32 1.30 26 PF 1 4.80 75.34 76.89 77.01 0.006682 1.55 3.10 2.00 12.7 PF 1 4.80 75.22 76.79 76.91 0.011611 1.56 3.08 5.40 11 Lat Struct 76.76 76.83 0.006302 1.13 3.49 6.80 5.4 PF 1 3.24 75.20 76.80 76.81 0.000253 0.36 9.10 10.00	incess avenue	59.8	1	4.00	(0.00)		20:00		٠		l		9 9 9
28 PF1 4.80 75.34 76.89 77.01 0.005682 1.55 3.10 2.00 2.00 12.7 PF1 4.80 75.22 76.79 76.91 0.011611 1.56 3.08 5.40 1.1	Action Condition	18.9	DE 1	4 80	75.40			77.20		2.50			0,66
26 PF1 4.80 75.34 76.89 77.01 0,000062 1.33 3.49 5.40 1.27 PF1 4.80 75.12 76.79 76.81 0,0011611 1.56 3.08 5.40 1.11 3.94 75.17 76.76 76.81 0,000253 0.35 9.10 10.00	HICESS SYCHOL	200				Ì				93.4			0.40
127 PF 1 Lat Struct 1.57 76.79 76.81 0.011611 1.56 3.08 5.40 1.1	Dogge summing	28	PE 1	4,80	75.34			10.77		1.00			
12.7 PF 1 4.80 75.22 76.79 76.91 0.011611 1.50 5.00 5.10 5.10 5.10 5.10 5.10 5.	Heese evenion	200	10000			l		7 9 9 9		000			O BR
11 Lat Struct 3.94 75.17 76.76 76.83 0.006302 1.13 3.49 6.80 0.0 pF 1 3.23 75.20 76.80 76.81 0.000253 0.36 9.10 10.00	ncess avenue	12.7	PF1	4.80				76.91	- 1	1.00		١	8
5.4 PF 1 3.94 75.17 76.76 76.83 0.006302 1.13 3.49 6.80	Acces authoriti	4.4		Lat Struct									1000
5.4 PF 1 3.94 75.17 76.76 75.80 76.81 0.000253 0.35 9.10 10.00	Incess evenue		10000			ľ		40.00	0000000	4.42		R RD	0.50
n peri 3.23 75.20 76.80 76.81 0.000253 0.35 9.10 10.00	ncess avenue	5.4	PF 1	3.94			100000000000000000000000000000000000000	70.03	0.000000	2		1	
	-		9 30	3 23	75.20		75.80	76.81	0.000253	0.36		10.00	0.12





River Sta Profile Q Total Min Ch El V/S. Elev Crif W S. E.G. Elev E.G. Elev E.G. Slope Vel Chnil Frow Area 1 op Width 59.8 PF 1 6.80 75.55 77.57 76.54 77.64 0.003920 1.16 5.87 7.20 38.2 PF 1 6.80 75.40 77.11 76.80 77.42 0.038274 2.44 2.78 6.20 26 PF 1 6.80 75.40 77.11 76.98 77.17 0.010484 2.12 3.21 2.00 12.7 PF 1 6.80 75.22 76.75 76.71 76.98 0.021258 2.14 3.18 5.60 11 Lat Shruct 75.17 76.18 76.76 76.76 76.76 76.76 76.76 76.76 76.76 76.76 76.76 76.76 76.76 76.77 76.77 76.77 76.77 76.77 76.77 76.77 76.77 76.77 76.77 76.78 76.76 <th>COLUMN TIME PO</th> <th>TOTAL CHICK</th> <th>Course of the same</th> <th></th> <th></th> <th>Contract and in Contract of the Contract of th</th> <th></th> <th></th> <th></th> <th></th> <th></th> <th>The same of the same</th> <th>۰</th>	COLUMN TIME PO	TOTAL CHICK	Course of the same			Contract and in Contract of the Contract of th						The same of the same	۰
59.8 PF 1 6.80 75.55 77.57 76.54 77.42 0.003820 1.16 5.87 7.20 38.2 PF 1 6.80 75.40 77.11 76.80 77.42 0.0038274 2.44 2.78 6.20 26 PF 1 6.80 75.34 76.35 76.71 76.98 0.01484 2.12 3.21 2.00 12.7 PF 1 6.80 75.22 76.75 76.71 76.98 0.021258 2.14 3.18 5.60 11 Lat Shuct 75.17 76.18 76.86 0.011850 2.19 2.90 2.00 5.4 PF 1 6.36 75.17 76.18 76.78 0.001160 0.69 8.70 10.00	Reach	River Sta	Profile	Q Total	MINCHE	W.S. Elev	Crit W.S.				Ĭ	10p Width	Proude # CRI
59.8 PF 1 6.80 75.50 77.57 76.54 77.64 0.003920 1.16 5.87 7.20 38.2 PF 1 6.80 75.40 77.11 76.80 77.42 0.038274 2.44 2.78 6.20 26 PF 1 6.80 75.34 76.75 76.71 76.98 0.010484 2.12 3.21 2.00 12.7 PF 1 6.80 75.22 76.75 76.71 76.98 0.021258 2.14 3.18 5.60 11 Lat Shuct 75.17 76.18 76.86 0.011850 2.19 2.90 2.00 5.4 PF 1 6.36 75.17 76.18 76.76 0.0011850 2.19 2.90 2.00 0 PF 1 6.36 75.17 76.16 76.76 76.76 76.76 76.77 76.77 76.76 76.77 76.76 76.77 76.77 76.76 76.76 76.77 76.77 76.76 76.77 <td< th=""><th></th><th>- North Control</th><th></th><th>(m3/s)</th><th>(E)</th><th>(H)</th><th></th><th></th><th></th><th></th><th></th><th>(m)</th><th></th></td<>		- North Control		(m3/s)	(E)	(H)						(m)	
38.2 PF 1 6.80 75.40 77.11 76.80 77.42 0.038274 2.44 2.78 6.20 6.20 2.60 2.60 75.34 76.95 77.17 0.010484 2.12 3.21 2.00 2.00 12.7 PF 1 6.80 75.22 76.75 76.71 76.98 0.021258 2.14 3.18 5.60 75.00 2.40 pF 1 6.36 75.17 76.62 76.18 76.86 0.011850 2.19 2.90 2.00 0.00 pF 1 6.36 75.17 76.62 76.16 76.76 0.001000 0.69 8.70 10.00	Section and section	0 00	1 20	8.80		77.57							
38.2 PF 1 6.80 75.34 76.95 77.17 0.010484 2.12 3.21 2.00 2.00 12.7 PF 1 6.80 75.32 76.75 76.71 76.98 0.021258 2.14 3.18 5.60 11.1 Lat Shuct 6.36 75.17 76.85 0.011850 2.19 2.90 2.00 0.00 pF 1 6.36 75.17 76.62 76.18 76.85 0.001000 0.69 8.70 10.00	anuska sesoul	0000		200		7 7 7							
26 PF 1 6.80 75.34 75.25 76.75 76.71 0.010484 2.12 3.21 2.00 12.7 PF 1 6.80 75.22 76.75 76.71 76.98 0.021258 2.14 3.18 5.60 11 Lat Shruct 75.17 76.68 76.18 76.86 0.011850 2.19 2.90 2.00 5.4 PF 1 6.36 75.17 76.16 76.76 76.76 76.76 9.001000 0.69 8.70 10.00	rincess avenue	38.2	PF 1	6.80	75.40	11.77		- 1	- 1	ı			
12.7 PFT 6.80 75.22 76.75 76.71 76.98 0.021258 2.14 3.18 5.60 11 Lat Shuct 6.36 75.17 76.62 76.18 76.86 0.011850 2.19 2.90 2.00 0 PFT 6.36 75.17 76.62 76.16 76.76 0.001000 0.69 8.70 10.00	dineses exenting	26	DE 1	6.80	75.34	78.95		77.17					
12.7 PF 1 6.80 75.22 76.75 76.71 76.96 0.021230 6.14 0.10 0.00 0.00 0.00 0.00 0.00 0.00 0	MINESS SVEHING	200		10000	STATE OF THE PARTY		ľ	400					
11 Lat Shruct 5.4 pF 1 6.36 75.17 76.62 76.18 76.86 0.011850 2.19 2.90 2.00 0 pF 1 5.99 75.20 76.76 76.16 76.78 0.001000 0.69 8.70 10.00	rincess avenue	12.7	PF 1	6.80	75.22	78.75		76.98		ľ		_	
5.4 PF 1 6.36 75.17 75.62 76.18 76.86 0.011850 2.19 2.90 2.00 0 PF 1 5.99 75.20 75.76 76.16 76.78 0.001000 0.69 8.70 10.00	rincess avenue	7		Lat Struct									
n pp 1 5.99 75.20 76.76 76.78 0.001000 0.69 8.70 10.00	rinches avenue	5.4	PF 1	6.36	75.17	76.62	76.18	76.85	0.011850	2.19	2.90		0.58
	incess avenue		DF 1	5.99	75.20	76.76	76.16	76.78	0.001000	0.69	8.70		0.24





VERSION	FEH CD-R	/ersion	3	exported at	10:25:13	GMT	Tue	05-Feb-13
CATCHMENT	GB	374600		SD 74600 42		orentale.	100000	-072/07/07
CENTROID	GB	375684		SD 75684 43				
AREA	1.61			770000000000000000000000000000000000000				
ALTBAR	98							
ASPBAR	284							
ASPVAR	0.37							
BFIHOST	0.435							_
DPLBAR	1.81							
DPSBAR	40.3						_	
FARL	0.995							
FPEXT	0.1073							
FPDBAR	0.798					_	_	
FPLOC	0.790						-	_
LDP	The second secon							
distribution of the second	3.28							
PROPWET	0.6							
RMED-1H	10.4							
RMED-1D	42.4							
RMED-2D	58.8							
SAAR	1222							
SAAR4170	1159							
SPRHOST	30.24							
URBCONC1990	0.325							
URBEXT1990	0.035							
URBLOC1990	0.455							
URBCONC2000	0.757							
URBEXT2000	0.098							
URBLOC2000	0.441							
С	-0.02592							_
D1	0.41741					Cri.	-	
D2	0.38874							
D3	0.43324					_	_	
E	0.30185							
F	2.45601						_	_
C(1 km)	-0.025						-	
D1(1 km)	0.405							
D2(1 km)	0.385	_				_		
D3(1 km)	0.437							
E(1 km)	0.301							
F(1 km)								
r(1 Mill)	2.458							
							-	
								1
								L. L.
			-					
Michael Lamber Catchment descr				Copyright un	der licence	from IoH		
Chatburn Beck a		nue		05/02/2013	mel			B1343
STREETH DOOR O	TITIOGGO AVE	an torus		0010272013	11/01			D 1343

VERSION Parameter	FEH CD-R	Version	3	exported at	10:31:37 Clitheroe rai	Maria de la constanta de la co	Tue	05-Feb-13		B1343
	Design rain	ifali			06/02/2013					
		nt in catchm	ent							
	Catchment		374600	442300	SD 74600 4	2300				
Catchment	1.61	100	km**2	1022.027	1551. Wilder					
Ouration=	6	1	(hours)							
bed durat	no									
Return per		1	(years)							
Annual ma	yes									
C	d1	d2	d3	e	t					
-0.02592	0.41741	0.38874	0.43324	0.30185	2.45601					
An areal re	duction fact	or of 0.976	nas been ap	plied to a po			vield a cate	hment desig	n rainfall of 77.8 mm.	
No warning	(s) or note(s	s) were pres	ent for this	alculation.		1 200	Jiero a cure	The transfer of the transfer o	Transaction of Transaction	
					sliding duration	ons				
			10		50		200	500		-
Duration	Duration	Duration			year rainfail					_
ninutes	hours	days	mm	mm	mm	mm	mm	mm		
15	And the second profession and the second	0.010417		16.44	22.52	- transfer to the same of the	Charles Inc.			-
30	0.25	being street them an experience of the last	The late of the la	21.21	28.57	-	36.06	and the second s		
45	0.75	The second second		24.57	32.77					
60	0.75	0.03123	21.92	27.24			the second secon	66.99		
75	1.25	TOTAL CONTRACTOR AND ADDRESS OF THE PARTY OF		29.51	36.09		the state of the s	72.52		
90				And the second s	38.88		58.74	77.09		
	1.5	0.0625	25.53	31.49	41.31		62	81.01		
105	1.75	Contraction of the Contraction o	27.05	33.26	43.47	Contract of the Contract of th	Charles and Advanced land			
120	2		28.43	34.88	45.44		67.49	87.58		
135	2.25	0.09375	29.71	36.36	47.24		69.87	90.41		
150	2.5	mer Section advantable for larger than the first of the contract of the contra	30.89	37.74	48.9		72.06			
165	2.75		32.01	39.03	50.46		74.1	95.43		
180	3	0.125	33.06	40.25	51.92		76.01	97.68		100
195	3.25	0.135417	34.05	41.4	53.3	The second second		99.8		
210	3.5		35	42.49	54.61	65.92	79.5	101.8		
225	3.75	0.15625	35.91	43.53	55.86	67.34	81.11	103.69		
240	4	0.166667	36.77	44.53	57.05			105.5		
255	4.25	0.177083	37.61	45.49	58.19		84.12	107.22		
270	4.5	0.1875	38.41	46.41	59.29		85.53	108.86		
285	4.75			47.3	60.35	The second second second	86.88	110.44		
300	5	0.208333	39.93	48.16	61.36	7,000,770	88.18	111.96		
315	5.25	0.21875	40.66	48.99	62.35		89.44			
330	5.5		41.36	49.79	63.3		90.65			
345	5.75	0.239583	42.04	50.57	64.22		91.83			
360	6	0.25	42.71	51,33	65.12	77.83	92.96	117.52		
375	The second second second	0.260417	43.35	52.07	65.99	78.81	94.07			
390		0.270833	43.98	52.78				118.8		
405	6.75	The second second			67.66			And the Control of th		
420				53.48	the state of the s					
435		0.291667		54.17	68.46		-	THE MANAGEMENT		
	The second secon	0.302083		54.83	69.25					
450	7.5			55.49	70.02		The second second			
465		0.322917		56.12	70.77					
480	70.70	0.333333		56,75	71.5		101.02			
495	8.25	the same of the sa		57.36	72.22			Annual Contract of the Contrac		
510		0.354167		57.96	72.92		102.8	A CONTRACTOR OF THE PARTY OF TH		
525	8.75		The second second	58.55	73.61					
540	9	CONTRACT STORY OF THE SEASON.		59.13	74.28			130.84		
555	9.25			59.69	74.94		105.33	131.79		
570		0.395833	50.56	60.25	75.59	89.6				
585	9.75				76.23					
600	10	0.416667	51.52		76.86					
615	10.25	0.427083	51,99	61.86	77.48			12/19/20/20/20/20/20		
630	10.5				78.08					
645	10.75			62.9	78.68			The second second second second		
660	- 11	the first time but the season was a season.		63.4	79.27	Control of the Control		A Secretaria de la Companya del Companya de la Companya del Companya de la Compan		
675	11.25	control where the has also street to be an extended		63.9	79.85		98.156003.44			
690	11.5			64.39	80.42	-				
705	11.75		54.66	64.87	80.98	Processor Salvanian Contraction of the Contraction				
720	12	to A remote that have provided in	The second secon	65.35	81.53					-
735	12.25			65.78	82.03					
750				The second secon			The second secon			
Annual Contract	12.5	and the second control of the contro		66.21	82.52		The street and street as			-
765	12.75			66.62	83		- The state of the			
780	13			67.04	83.48	7-	710070104000	The state of the s		
795	13.25	all colored in the last the first of the last th	the state of the latest and the late	67.45	83.94					
810	13.5			67.85	84.41	The second secon	The second secon			
825		0.572917		68.25	84.87	the second second second				
840	14	0.583333	58.02	68,64	85.32	100.42	118.13	146.35		