

Eric Wright Construction Ltd.

Clitheroe Care Home

Drainage Strategy

220018-JPS-XX-XX-RP-C-0001

Rev: P04

March 2023

Document History

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P04	Surface water drainage amended	JR	JP	14.06.2023
P03	Site layout amended	JR	JP	27.03.2023
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P01	Drainage Strategy	JR	JP	09.02.2023
Revision	Purpose Description	Originated	Authorised	Date

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1 Introduction

1.1 Commission

JP Structural Design were appointed by Eric Wright Construction Ltd. to produce a Drainage Strategy for a new build care home with access and car parking area at Clitheroe, Lancashire.

1.2 Limitations

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The findings of this Strategy have been based on data available at the time of the study and on the review of available information that has been undertaken to date. They relate to the current proposed layout as outlined in **Appendix A**. Should the proposed end use of the site change after the completion of this assessment, then the findings of this report will need to be reviewed and updated accordingly.

2 Existing Site and Proposed Development

2.1 Existing Site

The site is located on land off Dyke Nook, Clitheroe, Lancashire. The centre of the site is at National Grid Reference SD748407. The proposed site covers an area of approximately 0.990ha. See **Appendix B** for the Site Information Drawing.

The site is roughly triangular in shape and it is located to the south east of Clitheroe. The site is part of a wider proposed residential development within the area which will surround the site once completed. The site is currently agricultural land, there is a hedgerow in the north and a tree present in the centre of the site, there are no structures present.

A review of the topographical survey shows that the site falls in a northern direction. The survey indicates that the site has a high point of 103.850m (Above Ordnance Datum) AOD located in the south west of the site. The low point is located in the north west of the site at 101.300m AOD, with levels of 102.600m AOD and 103.280m AOD in the north east and south east corners respectively. Additionally, there is a 1.3-1.5m high earthworks mound located 15-20m from the west of the site boundary. The topographical survey of the site is provided in **Appendix C**.

2.2 Ground Conditions

The surface geology of the site has been reviewed from the British Geological Survey (BGS) online geology maps. The geology map indicates that the site is superficially underlain by "Till, Devensian - Diamicton. Sedimentary superficial deposit formed between 116 and 11.8 thousand years ago during the Quaternary period." The bedrock geology is described as "Clitheroe Limestone Formation and Hodder Mudstone Formation - Mudstone. Sedimentary bedrock formed between 346.7 and 337 million years ago during the Carboniferous period."

According to the Soilscales soils dataset (<http://www.landis.org.uk/soilscales/>), soil conditions at the site and within the surrounding area are slowly permeable seasonally wet acid loamy and clayey soils with impeded drainage.

E3P carried out soakaway testing on 19 December 2022 in accordance with BRE365 to determine infiltration rates of the site. A summary of the findings are provided in **Appendix D**. The testing was undertaken in three locations on site. The E3P report states the following:

"Within all three locations, soakaway testing failed, with the water level failing to soakaway below 75% effective storage. As such, soakaway drainage is not unlikely to be suitable on the site."

No groundwater was encountered within any of the exploratory holes.

2.3 Existing Waterbodies

There is an unnamed watercourse to the west of the site that discharges to Pendleton Brook.

There are no other water bodies within the immediate vicinity of the site.

2.4 Existing Drainage

Public sewer records obtained from United Utilities (UU) (refer to **Appendix E**) indicate that there are public sewers serving the existing residential areas to the north and west of the site but that there are no public sewers within the immediate vicinity of the site.

The site is undeveloped greenfield, given site topography and ground conditions, surface water runoff would be expected to flow overland in a north west direction.

The Coopers Chartered Consulting Engineers drawings 6263 / sp-a-03-1,2,3 and 4 for the Spine Road of Phase A of the wider development have been reviewed as part of this assessment (refer to **Appendix F**). The drawings indicate the following:

- A system comprising 300mm, 375mm and 450mm diameter surface water sewers situated within the proposed spine road as shown on the existing drainage layout in **Appendix G**. The system appears to discharge to the unnamed watercourse to the west of the site that ultimately discharges to Pendleton Brook.
- A system comprising 150mm, 225mm and 300mm diameter foul water sewers situated within the proposed spine road as shown on the existing drainage layout in **Appendix G**. The system appears to discharge to the 225mm / 300mm diameter public combined sewer situated within Littlemoor Road to the west of the site.

2.5 Existing Flood Risk

The Environment Agency Flood Map for Planning (Rivers and Sea) indicates the site is located in flood zone 1. Flood zones refer to the probability of river and sea flooding. Table 1 of the NPPG defines flood zones as follows:

- Flood zone 1: Low Probability. Land having a less than 1 in 1,000 annual probability of river or sea flooding.
- Flood zone 2: Medium Probability. Land having between a 1 in 100 and 1 in 1,000 annual probability of river flooding or between a 1 in 200 and 1 in 1,000 annual probability of sea flooding.
- Flood zone 3a: High Probability. Land having a 1 in 100 or greater annual probability of river flooding or a 1 in 200 or greater annual probability of sea flooding.
- Flood zone 3b: Functional Floodplain. Land where water has to flow or be stored in times of flood.

The management of surface water run-off generated by the post development site will be the principal flood risk associated with this scheme, therefore reduction of any flood risk is discussed in Section 3 of this report.

2.6 Proposed Development

The scheme consists of the construction of a new 2 storey 68 bed care home over in Clitheroe. The development will include a new building, landscaped areas and vehicular parking area. See **Appendix A** for proposed site layout.

3 Drainage Proposals

3.1 Foul Drainage

The proposed peak foul discharge generated by the development has been calculated based upon an occupancy rate of 1.5 persons per 1 bedroom, (allowing for residents and support staff) which equates to 102 persons. Therefore, allowing a typical usage of 350 l/person/day over a 24-hour day with a peak factor of 6, generates a peak foul flow of 2.5 l/s.

As the existing site is greenfield the peak foul flows from the proposed development will be greater than the existing.

It is proposed to discharge foul flows from the site to the existing manhole F10 via the existing 150mm diameter spur connection currently present in the south of the site as indicated on the preliminary drainage layout presented in **Appendix H**.

3.2 Surface Water Drainage

It is acknowledged that the satisfactory collection, control and discharge of storm water is now a principle planning and design consideration. Part H of the Building Regulations 2002 recommends that surface water run-off shall discharge to one of the following, listed in order of priority:

- a) an adequate soakaway or some other adequate infiltration system, or where that is not reasonably practicable,
- b) a watercourse, or, where that is not reasonably practicable,
- c) a sewer.

It is necessary to identify the most appropriate method of controlling and discharging surface water. The design should seek to improve the local run-off profile by using systems that can either attenuate run-off and reduce peak flow rates or positively impact on the existing flood profile.

3.2.1 Ground Infiltration Techniques

As detailed in Section 2, infiltration testing has been undertaken by E3P in accordance with the guidelines in BRE365. However, within all three locations, soakaway testing failed. As such the disposal of surface water via infiltration has been discounted for the site.

3.2.2 Discharge To Watercourse

It is therefore proposed to discharge surface water runoff from the site to the existing manhole S11 via the existing 150mm diameter spur connection currently present in the south of the site. This is indicated on the preliminary drainage layout presented in **Appendix H**. The existing system discharges to the unnamed watercourse to the west of the site that ultimately discharges to Pendleton Brook.

3.3 Surface Water Calculations

3.3.1 Proposed Discharge Rate

The greenfield runoff rate for the existing area have been calculated using the “Pre-development discharge” function of Causeway Flow. The following parameters were used in the calculation.

- The site has a total area of 0.990ha; however, the proposed developable area is taken as approximately 0.544ha. This excludes the areas of the site which are to remain undeveloped and are expected to continue to drain as existing (refer to **Appendix B**).
- SAAR (Standard Annual Average Rainfall) = 1203mm, Soil Index = 4, SPR (Surface Precipitation Rate) = 0.47, Region = 10.

The peak discharges of surface runoff from impermeable areas of the existing site are shown in the table 1 below:

Above Exceedance Probability of rainfall event	Existing Greenfield Runoff Rate (l/s)
1:1	4.2
QBAR	5.0
1:30	9.7
1:100	12.3

Table 1.0 – Peak Runoff Rate – Existing Site

It is proposed to restrict runoff from impermeable surfaces of the development to the existing greenfield QBAR rate of 5l/s.

3.3.2 Attenuation Storage

Attenuation storage will be provided to restrict surface water runoff generated across roofs and hardstanding.

The attenuation storage facility has been modelled using Causeway Flow (refer to **Appendix I**). The required storage volume has been sized to store the 1:100 rainfall event including a 50% increase in rainfall intensity to allow for climate change in accordance with Lead Local Flood Authority guidance. Based on a peak discharge rate of 5l/s, a total storage volume of 301m³ would be required. It is proposed that this storage is provided in a geo-cellular attenuation tank with a plan area of 198m² and a depth of 1.6m.

The proposed attenuation tank is to be located within the car park area to the south of the proposed building.

Additional storage is provided in the proposed network of pipes and manholes. A preliminary surface water drainage layout is provided in **Appendix H**.

4 Planning Requirements

4.1 Water Quality

The proposed sump gullies and proposed vortex flow control catch pit manhole are deemed to be sufficient to remove the suspended sediments from the roof and car park surface water for a development of this size and nature.

4.2 Exceedance Events

Flooding is not expected to occur in the 1:100 year rainfall event plus 50% climate change for the site. It is anticipated that flood flows from rainfall events above this will be directed towards the access road and car parking areas respectively, with the site being profiled to ensure that flood flows are directed away from built development.

4.3 O&M Manuals

During the detail design stage & construction, full details of the final design will be submitted and included in the O&M manuals to ensure the drainage system is regularly maintained with particular regards to the surface water system. This will include manufacturer's guidelines for maintenance and replacement and full details of the flow control device as well as means to operate the drain down features in a blockage situation.

5 Conclusions

The proposed development is not expected to be affected by general objections in respect to draining the site. There will be suitable conditions imposed to ensure that the drainage proposals are designed and constructed in accordance with relevant statutory requirements, including Building Regulations 2010 and the requirements of Lancashire Lead Local Flood Authority.

Appendix A – Proposed Layout



- BOUNDARY TREATMENTS KEY:
- LOW HEIGHT STONE WALL
 - 1800MM HIGH METAL HOOP TOP RAILINGS
 - 1800MM HIGH CLOSE BOARDED TIMBER FENCE
 - EXISTING GREEN MESH FENCE TO SCHOOL BOUNDARY
 - HEDGING
 - NEW 1800MM HIGH MESH FENCING

NOTE: PLAN PRODUCED USING ALMAGATED INFORMATION FROM PLANNING APPLICATIONS:

21/0957
22/0116
21/0951

AND SUBJECT TO CHANGE.

PLEASE SEE DRAWING BY SUMO SERVICES SU-MO-10800 FOR LEVEL INFORMATION WITHIN RED LINE BOUNDARY.

NOTE: For final landscaping proposals refer to TEL Landscape drawings ref MR22-142/101 & MR22-142/102.

DRAWING REVISIONS				
REV	DESCRIPTION	DATE	BY	CHK
A	Drawings updated to suit general comments from client. Amendments include riser positions being indicated, additional doors being added & re-configuration of the servery and dining layout.	18.01.23	JA	TE
B	Service road reduced to single lane at a width of 3.7m. Additional path added at the side of service road for staff access.	10.02.23	JA	TE
C	Close boarded fencing to the east boundary omitted and replaced with metal mesh fencing. Change made to suit client comments.	20.02.23	JA	TE
D	Proposed sub-station location indicated on drawing in green hatch with annotation & dimensions to suit.	07.03.23	JA	TE
E	Footpath location amended.	16.03.23	JA	TE
F	General amendments made including wall vent locations indicatively shown on drawing. PV panel numbers updated as guided by M&E Consultant. Landscaping co-ordinated to suit TEL Landscape drawings.	24.03.23	JA	TE

NOTES

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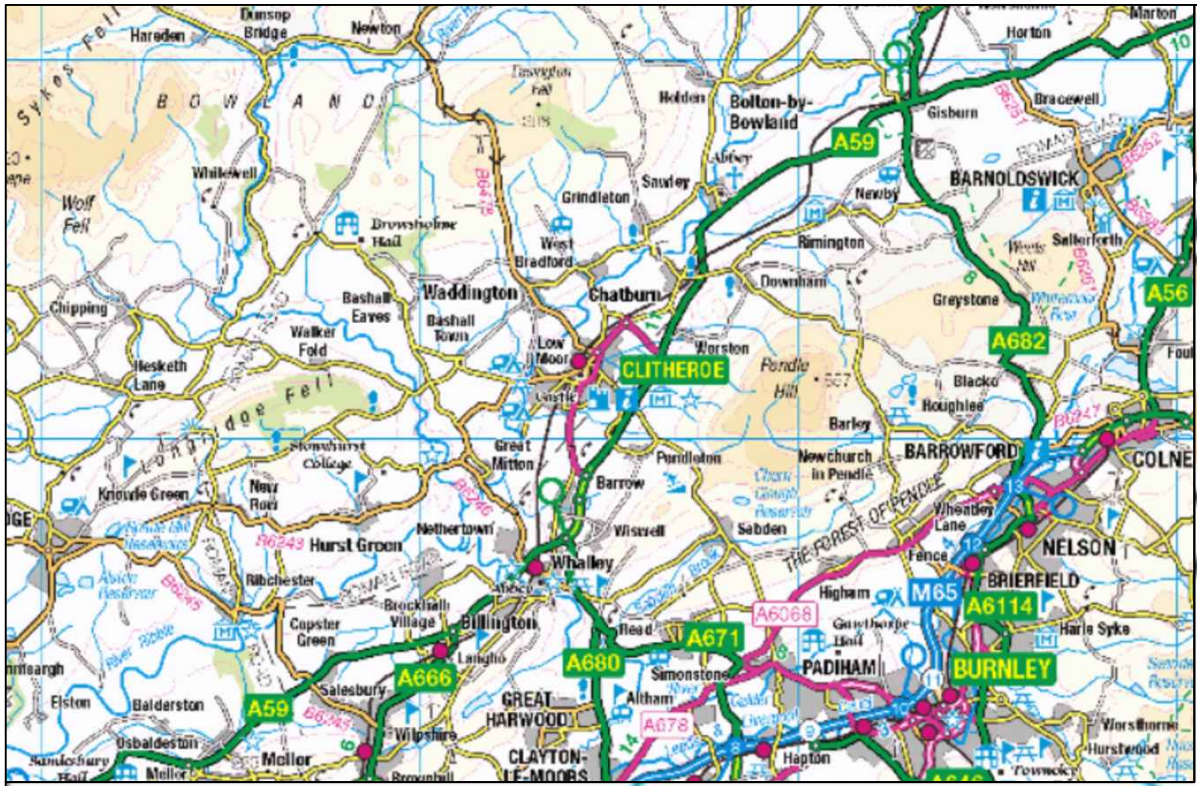
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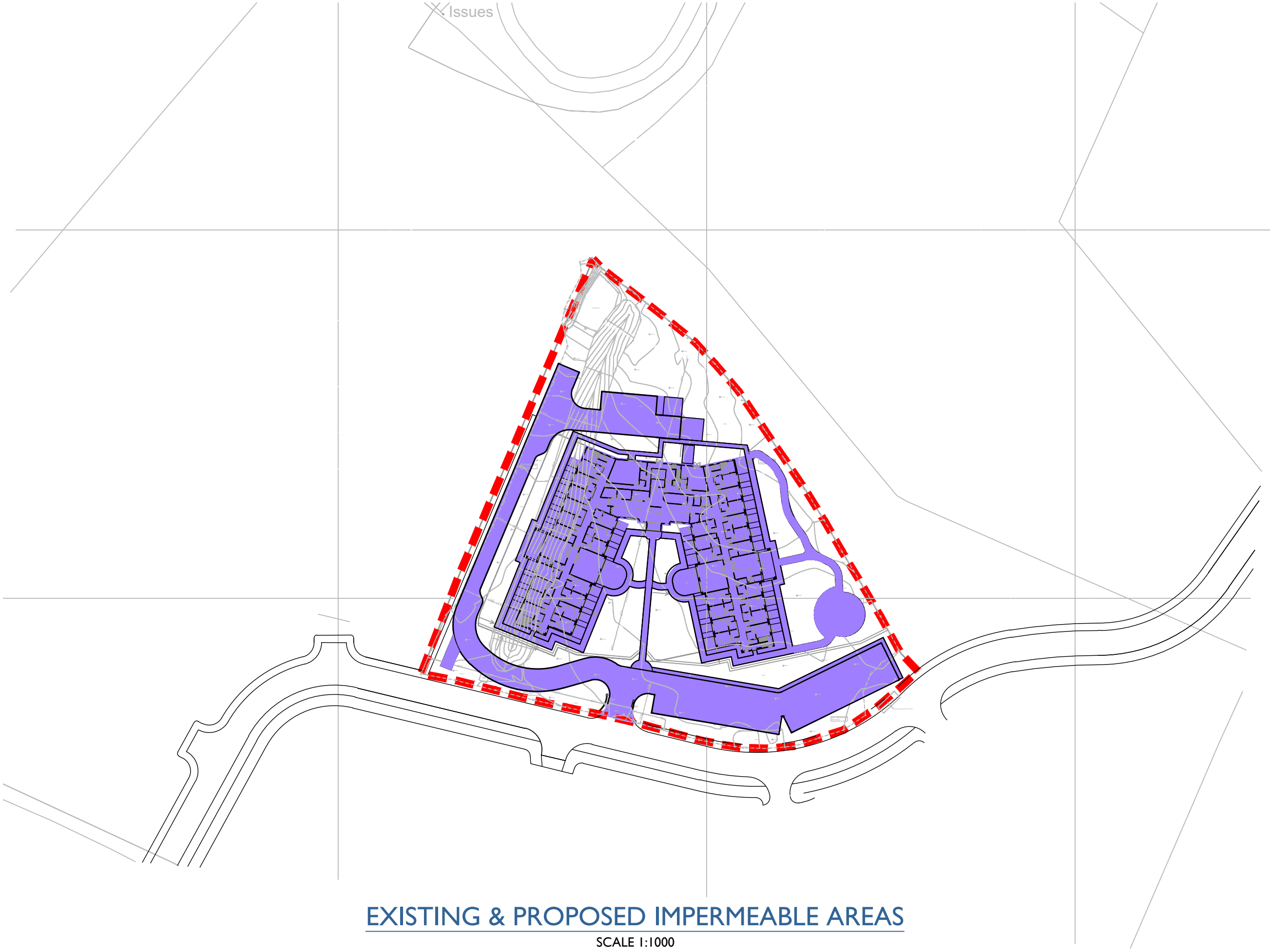
01904 544 400
dwa@dwa-architects.co.uk
www.dwa-architects.co.uk

CLIENT Eric Wright Group			
PROJECT Proposed Care Home, Standen Central Site, Clitheroe			
DRAWING TITLE Proposed Site Plan			
DWA PROJECT NO. G5709	DWA DWG NO. 192	REV F	
DRAWING STATUS PLANNING			
SCALE As indicated @ A1	DATE 21.12.22	DRAWN BY JA	CHECKED BY TE
BIM JOB NO. 220018		SUITABILITY CODE SUITABILITY DESCRIPTION	
DOCUMENT NAME (BS EN ISO 19650) 220018-DWA-XX-XX-DR-A-192-F-Proposed Site Plan			

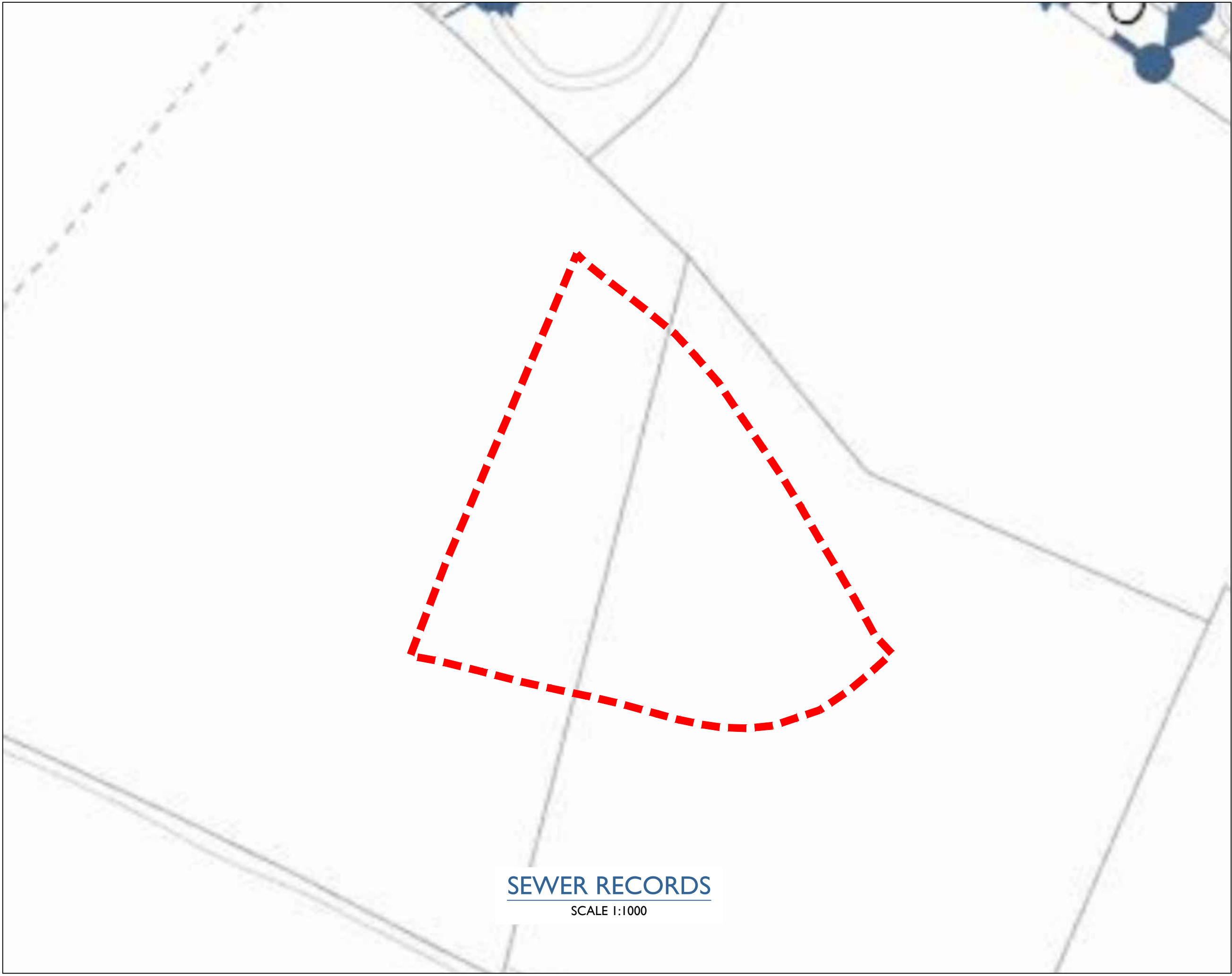
Appendix B – Site Information Drawing



LOCATION PLAN
SCALE 1:200,000 / 5,000



EXISTING & PROPOSED IMPERMEABLE AREAS
SCALE 1:1000



SEWER RECORDS
SCALE 1:1000



SATELITE IMAGE OF THE SITE
SCALE 1:1000

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SITE CO-ORDINATES
OS X (Easting) 374889
OS Y (Northings) 440726
Nearest Post Code BB7 1FZ
Nat Grid SD748407 / SD7488940726



AREAS	
	SITE BOUNDARY 9,900m ² (0.990 ha)
	ADDITIONAL IMPERMEABLE AREA 5,440m ² (0.544 ha)

PO2		SITE LAYOUT AMENDED		JR	RH	MM	27.03.2023
REV		DESCRIPTION		BY	CHK	APR	DATE

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PURPOSE OF ISSUE		STAGE 2		STATUS	
PROJECT		CLITHEROE CARE HOME		S2	
TITLE		DRAINAGE SCHEME SITE INFORMATION			
CLIENT		ERIC WRIGHT CONSTRUCTION LTD			
DRAWN BY	CHECKED BY	APPROVED BY			
JR	RH	MM			
DATE	SCALE (@ A1)	PROJECT NUMBER			
08.02.2023	AS SHOWN	113001			
DRAWING NUMBER		REV			
220018-JPS-ZZ-ZZ-DR-C-00500		P02			

Appendix C – Topographic Survey

Appendix D – Soakaway Test Summary

3.12. SOIL INFILTRATION

In-situ BRE 365 Soakaway tests were undertaken within trial pits completed as SA101-SA103.

The results are presented in Table 3.7 below and the test certificates are included within Appendix IX.

TABLE 3.7 BRE365 SOAKAWAY TESTING RESULTS

LOCATION	DEPTH (m)	MATERIAL	TEST NO.	SOIL INFILTRATION RATE (m/s)
SA101/TP101b	2.10	Gravelly CLAY	Test No.1	N/A
SA102/TP102	1.70	Slightly sandy gravelly CLAY	Test No.1	N/A
SA103/TP103	1.90	Sandy gravelly CLAY	Test No.1	N/A

All three tests did not record a sufficient fall in water level to allow reliable calculation of the infiltration rate.

The tests suggest the cohesive drift deposits are unlikely to be suitable for soakaway drainage.

However, the application of soakaway drainage will ultimately be dependent on the specific requirements of the development. All soakaways should be designed in accordance with BRE Special Digest 365 – *Soakaway Design*.

3.13. SOIL PLASTICITY

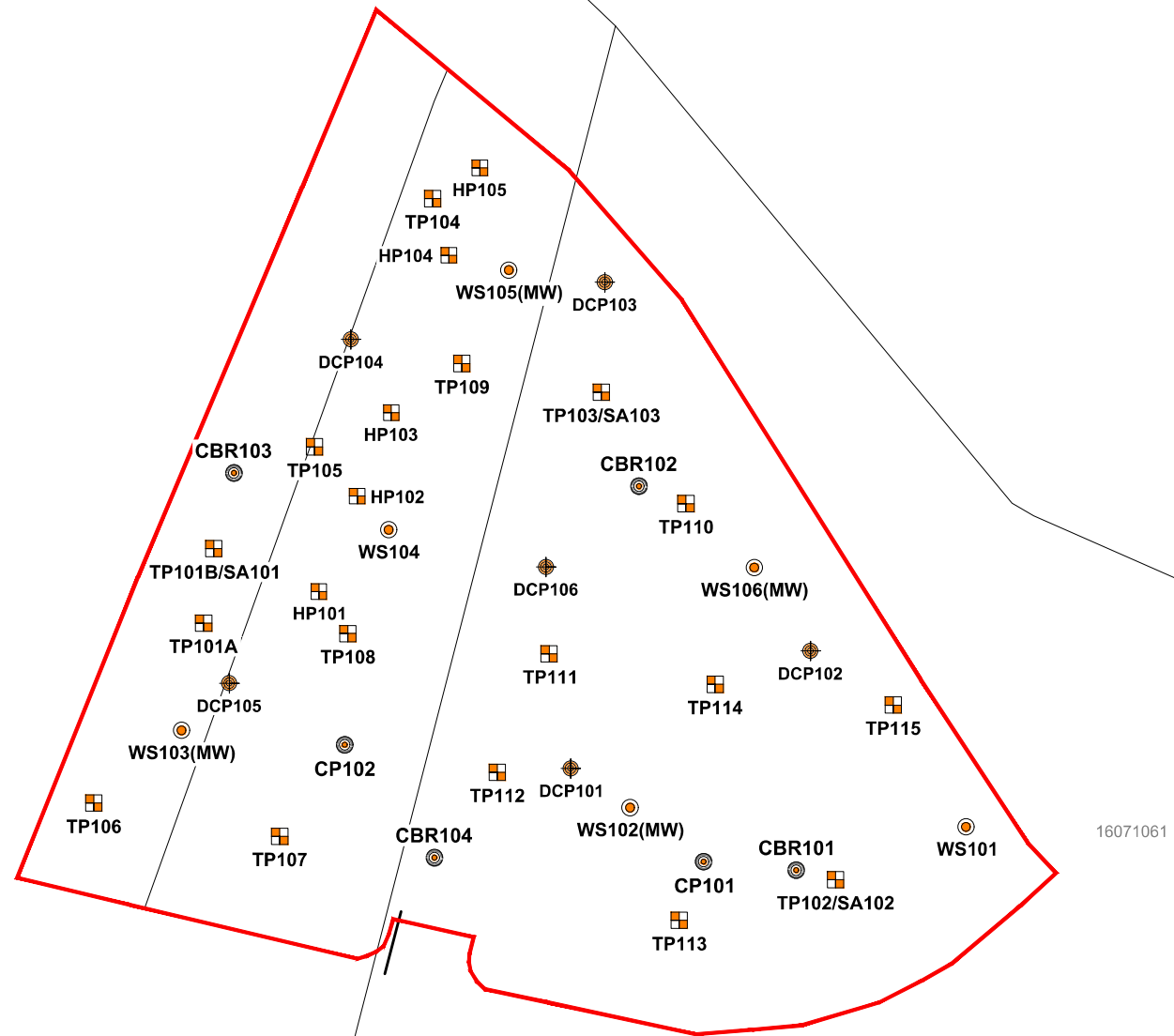
The Atterberg limits determinations, summarised in Table 3.8, show the clay to be of predominantly low plasticity with discrete areas of moderate plasticity clay.

TABLE 3.8 SUMMARY OF PLASTICITY INDEX TEST RESULTS

LOCATION	DEPTH (m)	NATURAL MOISTURE CONTENT (%)	PLASTIC LIMIT (%)	LIQUID LIMIT (%)	PLASTICITY INDEX (%)	PASSING 425 µm SIEVE (%)	MODIFIED PLASTICITY INDEX	NHBC VOLUME CHANGE POTENTIAL
WS104	1.00	13	14	29	15	62	9.3	Low
WS105	1.00	16	15	32	17	64	10.88	Low
WS102	2.00	16	13	27	14	60	8.4	Low
WS101	2.00	14	15	31	16	73	11.68	Low
CP101	5.00	11	13	28	15	64	9.6	Low
CP102	1.20	30	23	47	24	89	21.36	Medium
CP102	3.00	11	13	27	14	65	9.1	Low

The results of the Atterberg limits testing confirmed that the soils would be deemed to be “Low Potential” in accordance with the classification system utilised by the LABC/NHBC industry guidance.





- Location Symbols
- Approximate Window Sample Probehole Location
 - Approximate Trial Pit Location
 - Approximate Cable Percussive Borehole Location
 - Approximate Soakaway Test Location
 - Approximate Hand Dug Pit Location
 - Approximate California Bearing Ratio Test Location
 - Approximate Dynamic Cone Penetrometer Test Location

Notes:

Client:

Eric Wright

Job No:

16-499

Date:

06.02.2023

Drawing No:

005

Scale:

NTS @ A3

 Environmental Engineering Partnership Ltd
Taylor Road, Trafford Park
Urmston, Manchester, M41 7JO
Tel: 0161 707 9612
E-mail: info@e3p.co.uk
Website: www.e3p.co.uk

P1	REVB	06.02.2023	OW	EC
P1	REVA	16.12.2022	OW	EC
Phase	Issue	Date	Drawn	Checked

Job Title:

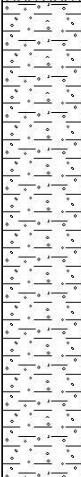
Standen Central

Drawing Title:

Exploratory Hole Location Plan

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Project Name: Standen Central	Project No. 16499	Co-ords: 374848.00 - 440718.00 Level:	Date 19/12/2022
Location: Clitheroe	Dimensions (m): 1.90 0.70		Scale 1:30
Client: Eric Wright	Depth 2.10		Logged E. Canham

Water Strike	Samples & In Situ Testing			Depth (m)	Level (m)	Legend	Stratum Description	
	Depth	Type	Results					
				0.20			Brown sandy CLAY with occasional rootlets. (Topsoil)	
				2.10			Very stiff greyish brown mottled orange sandy gravelly CLAY with frequent cobbles and occasional boulders. Gravel is fine to coarse subangular to subrounded of mudstone. Cobbles and boulders are subrounded mudstone.	1 2 3 4
							End of Pit at 2.10m	

Trial Pit Photographs



Soakaway 101/ Trial Pit 101b



Soakaway 101/ Trial Pit 101b Spoil

Remarks: 1. Complete 2. Soakaway test completed

Stability: Stable.

Project Name: Standen Central

Project No.
16499

Co-ords: 374927.00 - 440675.00
Level:

Date
19/12/2022

Location: Clitheroe

Dimensions (m): 1.90

Scale
1:30

Client: Eric Wright

Depth
1.70

0.70

Logged
E. Canham

Water Strike	Samples & In Situ Testing			Depth (m)	Level (m)	Legend	Stratum Description	
	Depth	Type	Results					
				0.30			Dark brown silty sandy CLAY with occasional rootlets. (Topsoil)	
	0.60	HVP	66				Firm light brown slightly silty slightly sandy CLAY with occasional rootlets.	
	0.80	ES		1.00			Firm to stiff dark greyish brown slightly sandy gravelly CLAY with frequent cobbles and occasional boulders. Gravel is fine to coarse subangular to subrounded of mudstone. Cobbles and boulders are subrounded mudstone.	1
				1.70				
							End of Pit at 1.70m	2
								3
								4

Trial Pit Photographs



Soakaway 102/ Trial Pit 102

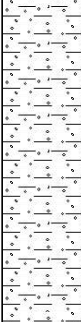


Trial Pit 102/ Soakaway 102 Spoil

Remarks: 1. Complete 2. Soakaway test completed

Stability: Stable.

Project Name: Standen Central	Project No. 16499	Co-ords: 374901.00 - 440746.00 Level:	Date 19/12/2022
Location: Clitheroe	Dimensions (m): 1.90 Depth 1.90		Scale 1:30
Client: Eric Wright			Logged E. Canham

Water Strike	Samples & In Situ Testing			Depth (m)	Level (m)	Legend	Stratum Description	
	Depth	Type	Results					
	0.25	ES		0.30			Dark brown silty sandy CLAY with occasional rootlets. (Topsoil)	
	0.50	HVP	98	0.60			Firm to stiff greyish brown mottled orange slightly silty sandy CLAY with occasional rootlets.	
				1.90			Very stiff greyish brown sandy gravelly CLAY with frequent cobbles and occasional large boulders. Gravel is fine to coarse subrounded to rounded of mudstone. Cobbles and boulders are subrounded of mudstone.	1
							End of Pit at 1.90m	2
								3
								4

Trial Pit Photographs



Trial Pit 103/ Soakaway 103



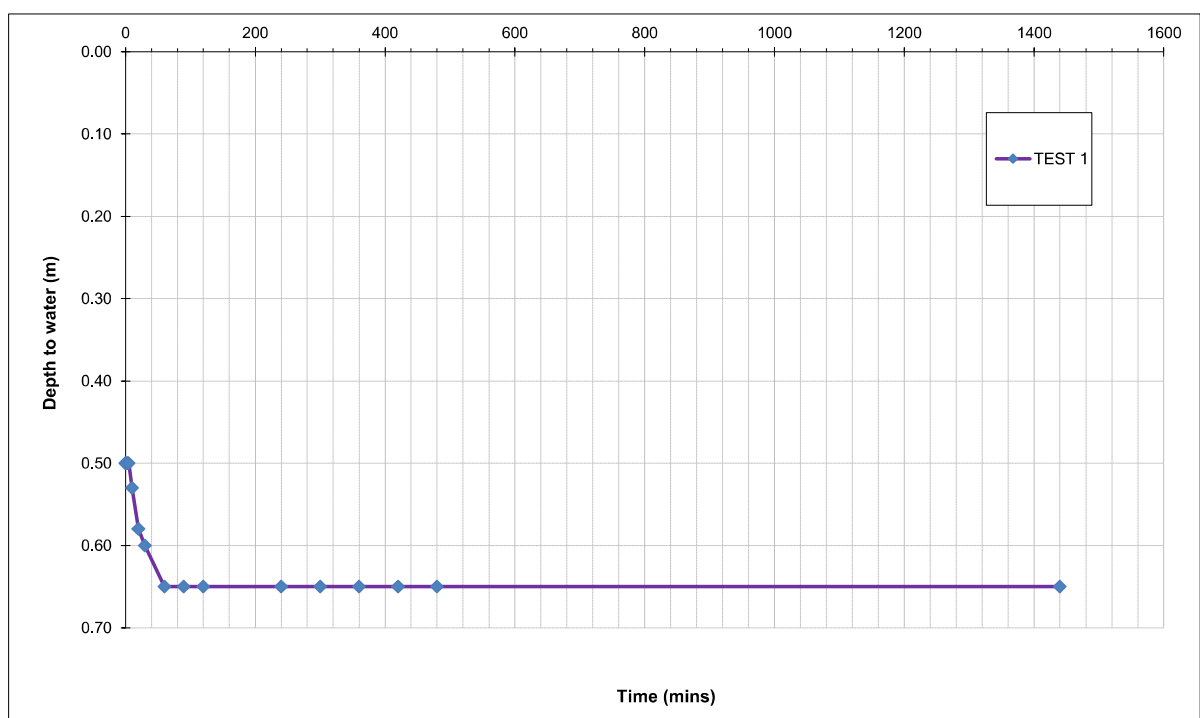
Soakaway 103/ Trial Pit 103 Spoil

Remarks: 1. Complete 2. Soakaway test completed

Stability: Stable.

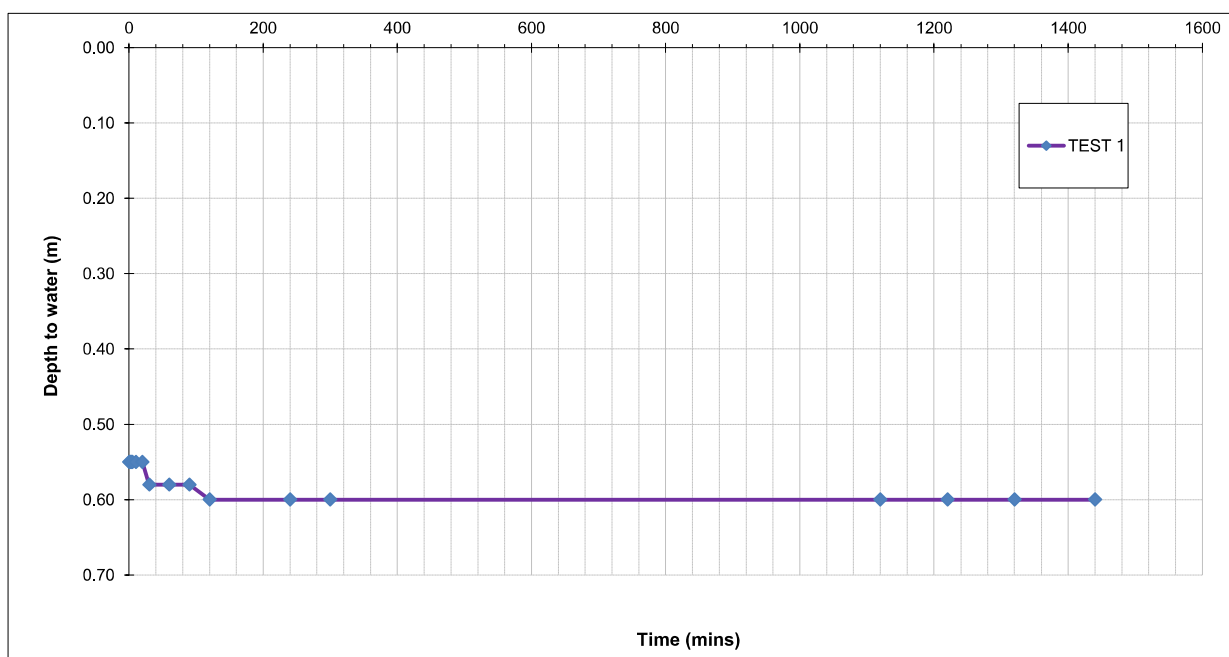
		Site: Standen Central Job Number: 16-499 Date of Test: 19/12/2022		Trial Pit Number: 101 Length: 2.00 m Width: 0.60 m Depth: 1.90 m Groundwater Level: N/A m		
Test 1 did not reach 75% or 25% effective storgae depth, therefore an infiltration rate could not be calculated.	TEST 1		TEST 2		TEST 3	
	Time(min)	Depth to Water (m)	Time(min)	Depth to Water (m)	Time(min)	Depth to Water (m)
	0	0.50				
	1	0.50				
	2	0.50				
	3	0.50				
	4	0.50				
	5	0.50				
	10	0.53				
	20	0.58				
	30	0.60				
	60	0.65				
	90	0.65				
	120	0.65				
	240.00	0.65				
	300.00	0.65				
	360.00	0.65				
420.00	0.65					
480.00	0.65					
1440.00	0.65					
Effective Storage Depth	m	1.40				
75% Effective Storage Depth	m	1.05				
(i.e. depth below GL)	m	0.85				
25% Effective Storage Depth	m	0.35				
(i.e. depth below GL)	m	1.55				
Effective Storage Depth 75%-25%	m	0.70				
Time to fall to 75% effective depth	mins	N/A				
Time to fall to 25% effective depth	mins	N/A				
V (75%-25%)	m3	0.84				
a (50%)	m2	4.84				
t (75%-25%)	mins	N/A				
SOIL INFILTRATION RATE	m/s	N/A				

DESIGN SOIL INFILTRATION RATE, f	N/A
---	------------



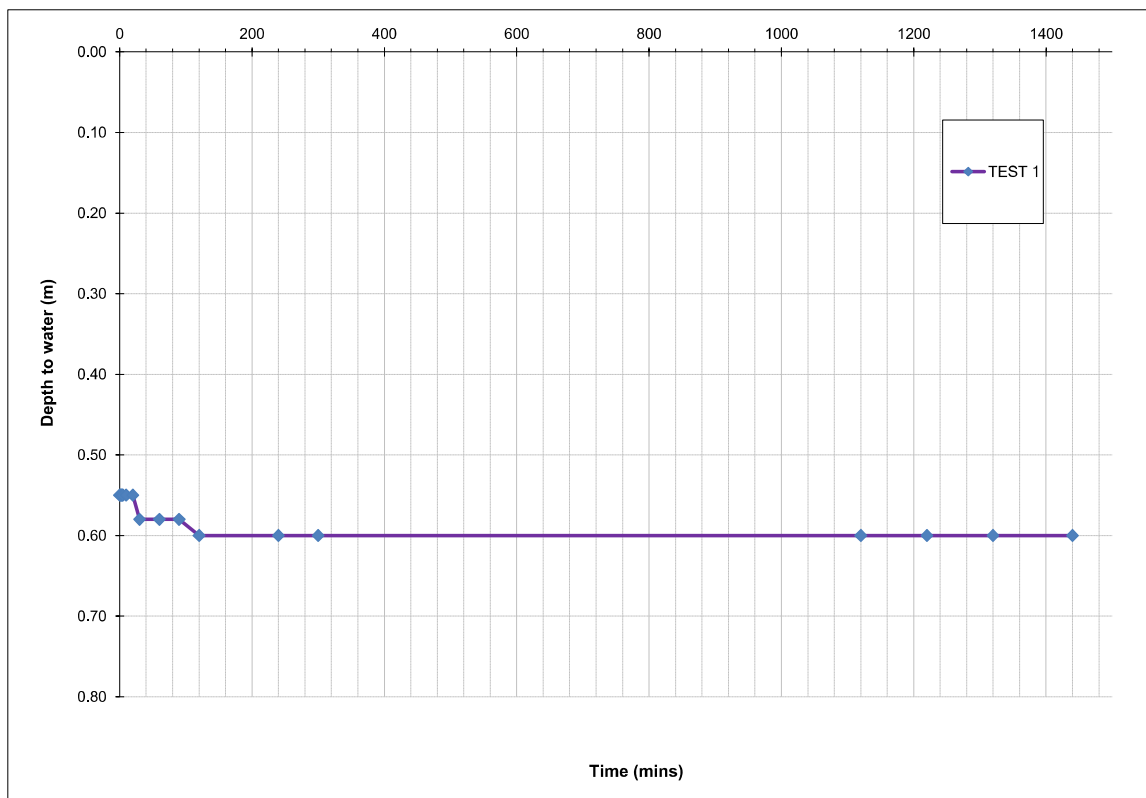
		Site: Standen Central Job Number: 16-499 Date of Test: 19/12/2022		Trial Pit Number: 102 Length: 1.75 m Width: 0.69 m Depth: 1.90 m Groundwater Level: N/A m			
Test 1 did not reach 75% or 25% effective storgae depth, therefore an infiltration rate could not be calculated.		TEST 1		TEST 2		TEST 3	
		Time(min)	Depth to Water (m)	Time(min)	Depth to Water (m)	Time(min)	Depth to Water (m)
		0	0.55				
		1	0.55				
		2	0.55				
		3	0.55				
		4	0.55				
		5	0.55				
		10	0.55				
		20	0.55				
		30	0.58				
		60	0.58				
		90	0.58				
		120	0.60				
		240	0.6				
		300.00	0.6				
	1120.00	0.60					
	1220.00	0.60					
	1320.00	0.60					
	1440.00	0.60					
Effective Storage Depth	m		1.35				
75% Effective Storage Depth	m		1.01				
(i.e. depth below GL)	m		0.89				
25% Effective Storage Depth	m		0.34				
(i.e. depth below GL)	m		1.56				
Effective Storage Depth 75%-25%	m		0.68				
Time to fall to 75% effective depth	mins		N/A				
Time to fall to 25% effective depth	mins		N/A				
V (75%-25%)	m3		0.82				
a (50%)	m2		4.50				
t (75%-25%)	mins		N/A				
SOIL INFILTRATION RATE	m/s		N/A				

DESIGN SOIL INFILTRATION RATE, f	N/A
---	-----



		Site: Standen Central Job Number: 16-499 Date of Test: 19/12/2022		Trial Pit Number: 103 Length: 1.75 m Width: 0.69 m Depth: 1.90 m Groundwater Level: N/A m	
Test 1 did not reach 75% or 25% effective storage depth, therefore an infiltration rate could not be calculated.	TEST 1		TEST 2		TEST 3
	Time(min)	Depth to Water (m)	Time(min)	Depth to Water (m)	Time(min) Depth to Water (m)
	0.00	0.55			
	1	0.55			
	2	0.55			
	3	0.55			
	4	0.55			
	5	0.55			
	10	0.55			
	20	0.55			
	30	0.58			
	60	0.58			
	90	0.58			
	120	0.60			
	240	0.6			
	300	0.6			
	1120.00	0.60			
	1220.00	0.60			
1320.00	0.60				
1440.00	0.60				
Effective Storage Depth	m	1.35			
75% Effective Storage Depth	m	1.01			
(i.e. depth below GL)	m	0.89			
25% Effective Storage Depth	m	0.34			
(i.e. depth below GL)	m	1.56			
Effective Storage Depth 75%-25%	m	0.68			
Time to fall to 75% effective depth	mins	N/A			
Time to fall to 25% effective depth	mins	N/A			
V (75%-25%)	m3	0.82			
a (50%)	m2	4.50			
t (75%-25%)	mins	N/A			
SOIL INFILTRATION RATE	m/s	N/A			

DESIGN SOIL INFILTRATION RATE, f	N/A
----------------------------------	-----



Appendix E – Public Sewer Record

JP STRUCTURAL DESIGN LTD

Regus House
Chester Business Park, JP STRUCTURAL DESIGN LTD
Chester,
CH4 9QR

FAO:

How to contact us:

United Utilities Water Limited
Property Searches
Haweswater House
Lingley Mere Business Park
Great Sankey
Warrington
WA5 3LP

Telephone: 0370 7510101

E-mail: propertysearches@uuplc.co.uk

Your Ref: 113001
Our Ref: UUPS-ORD-460622
Date: 27/01/2023

Dear Sirs

Location: Clitheroe Care Home

I acknowledge with thanks your request dated 27/01/2023 for information on the location of our services.

Please find enclosed plans showing the approximate position of United Utilities' apparatus known to be in the vicinity of this site.

The enclosed plans are being provided to you subject to the United Utilities terms and conditions for both the wastewater and water distribution plans which are shown attached.

If you are planning works anywhere in the North West, please read United Utilities' access statement before you start work to check how it will affect our network. <http://www.unitedutilities.com/work-near-asset.aspx>.

I trust the above meets with your requirements and look forward to hearing from you should you need anything further.

If you have any queries regarding this matter please [contact us](#).

Yours Faithfully,



Karen McCormack
Property Searches Manager

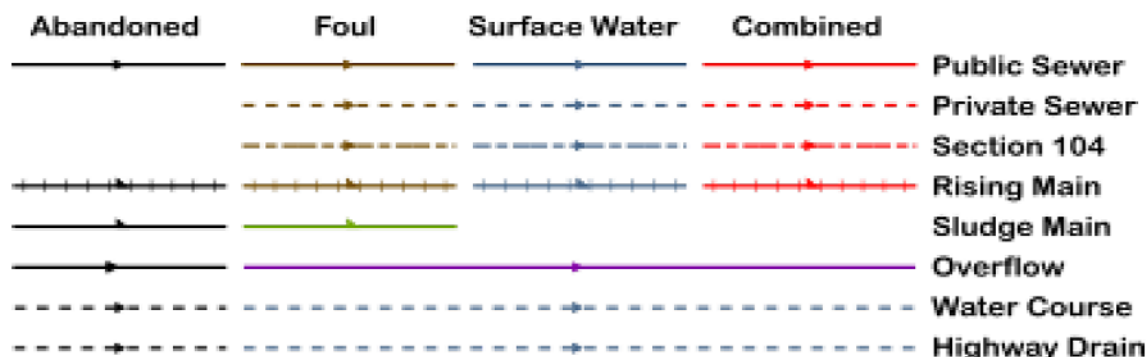
TERMS AND CONDITIONS - WASTEWATER AND WATER DISTRIBUTION PLANS

These provisions apply to the public sewerage, water distribution and telemetry systems (including sewers which are the subject of an agreement under Section 104 of the Water Industry Act 1991 and mains installed in accordance with the agreement for the self construction of water mains) (UUWL apparatus) of United Utilities Water Limited "(UUWL)".

TERMS AND CONDITIONS:

- This Map and any information supplied with it is issued subject to the provisions contained below, to the exclusion of all others and no party relies upon any representation, warranty, collateral contract or other assurance of any person (whether party to this agreement or not) that is not set out in this agreement or the documents referred to in it.
- This Map and any information supplied with it is provided for general guidance only and no representation, undertaking or warranty as to its accuracy, completeness or being up to date is given or implied.
- In particular, the position and depth of any UUWL apparatus shown on the Map are approximate only. UUWL strongly recommends that a comprehensive survey is undertaken in addition to reviewing this Map to determine and ensure the precise location of any UUWL apparatus. The exact location, positions and depths should be obtained by excavation trial holes.
- The location and position of private drains, private sewers and service pipes to properties are not normally shown on this Map but their presence must be anticipated and accounted for and you are strongly advised to carry out your own further enquiries and investigations in order to locate the same.
- The position and depth of UUWL apparatus is subject to change and therefore this Map is issued subject to any removal or change in location of the same. The onus is entirely upon you to confirm whether any changes to the Map have been made subsequent to issue and prior to any works being carried out.
- This Map and any information shown on it or provided with it must not be relied upon in the event of any development, construction or other works (including but not limited to any excavations) in the vicinity of UUWL apparatus or for the purpose of determining the suitability of a point of connection to the sewerage or other distribution systems.
- No person or legal entity, including any company shall be relieved from any liability howsoever and whensoever arising for any damage caused to UUWL apparatus by reason of the actual position and/or depths of UUWL apparatus being different from those shown on the Map and any information supplied with it.
- If any provision contained herein is or becomes legally invalid or unenforceable, it will be taken to be severed from the remaining provisions which shall be unaffected and continue in full force and affect.
- This agreement shall be governed by English law and all parties submit to the exclusive jurisdiction of the English courts, save that nothing will prevent UUWL from bringing proceedings in any other competent jurisdiction, whether concurrently or otherwise.

Wastewater Symbolology



All point assets follow the standard colour convention: **red** – combined **brown** - foul
blue – surface water **purple** - overflow

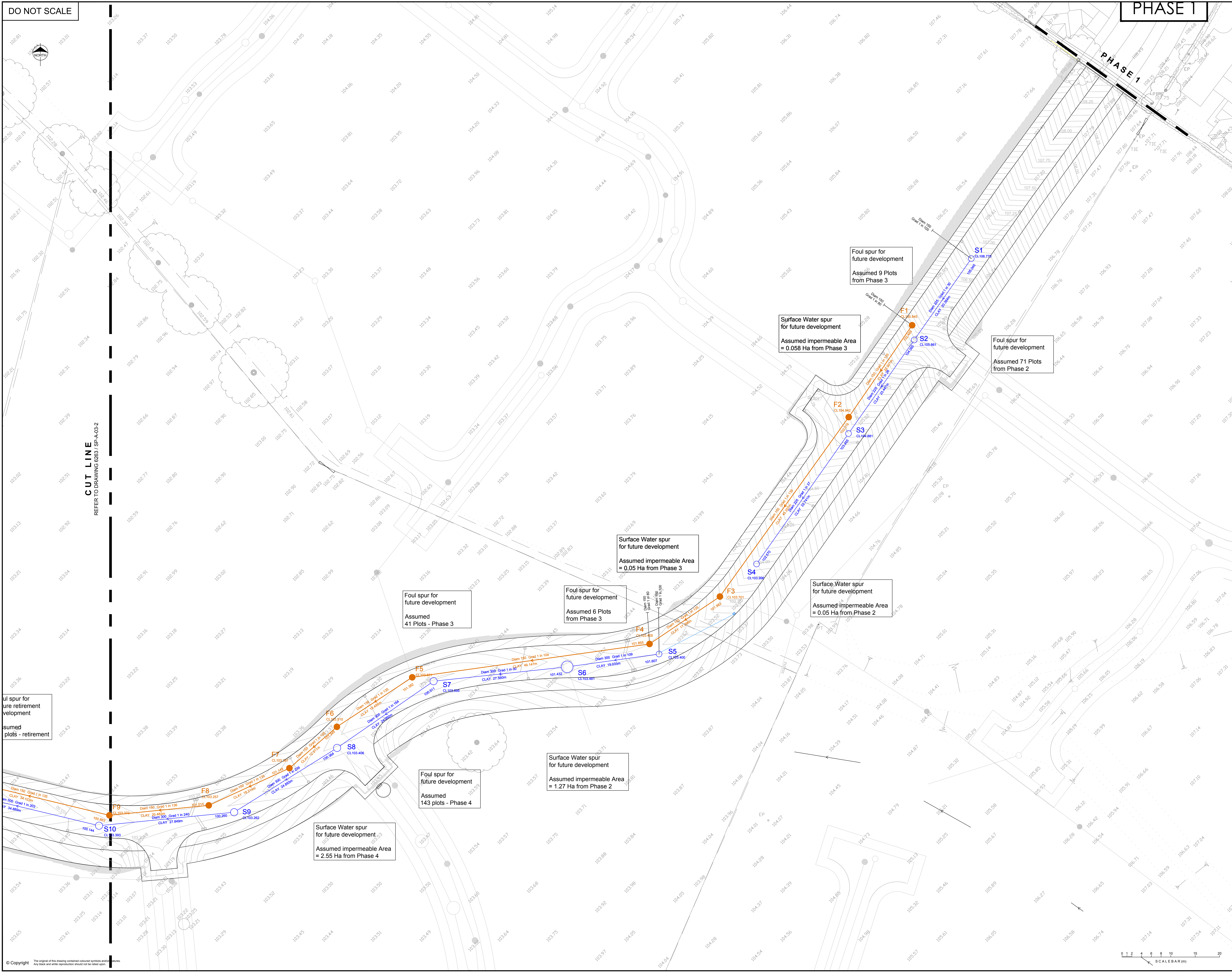
Manhole	Side Entry Manhole
Head of System	Outfall
Extent of Survey	Screen Chamber
Rodding Eye	Inspection Chamber
Inlet	Bifurcation Chamber
Discharge Point	Lamp Hole
Vortex	T Junction / Saddle
Penstock	Catchpit
Washout Chamber	Valve Chamber
Valve	Vent Column
Air Valve	Vortex Chamber
Non Return Valve	Penstock Chamber
Soakaway	Network Storage Tank
Gully	Sewer Overflow
Cascade	Ww Treatment Works
Flow Meter	Ww Pumping Station
Hatch Box	Septic Tank
Oil Interceptor	Control Kiosk
Summit	
Drop Shaft	Change of Characteristic
Orifice Plate	

Scale: 1:5329 Date: 27/01/2023	SEWER RECORDS	 Water for the North West
Address or Site Reference: Clitheroe Care Home Printed by: Property Searches		

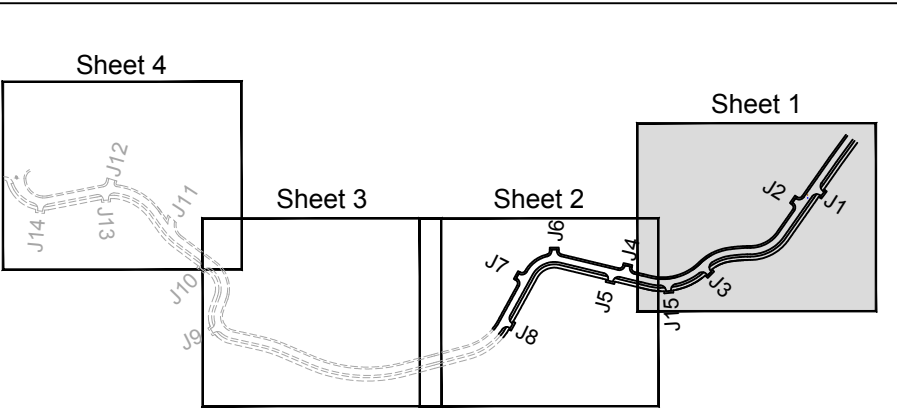
The position of the underground apparatus shown on this plan is approximate only and is given in accordance with the best information currently available. United Utilities Water will not accept liability for any loss or damage caused by the actual position being different from those shown.

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Appendix F – Wider Development Drainage



- Notes**
- Setting out shall be undertaken using only the information given. Distances should not be scaled from this drawing.
 - All sewers shall be constructed in accordance with Sewers for Adoption 6th Edition and United Utilities Details & Guidelines.
 - The minimum gravity pipe diameter under adoptable highways shall be 150mm.
 - It is the responsibility of the Contractor to verify all information given with regards to existing services and drainage connections etc. prior to commencing the works. The rates shall include for hand dig around services where necessary. The Contractor shall adhere to the CDM Regulations at all times.
 - The outsides of all sewers shall be a minimum of 1.0m from kerb lines and the outside of manholes shall be a minimum of 0.5m from kerb lines.
 - Existing flows in watercourses, sewers and land drains shall be maintained at all times.
 - Only trained personnel shall be permitted to enter confined spaces.
 - All materials to bear the relevant B.S. Kitemark and comply fully with the specifications. All concrete & concrete products must use Sulphate resistant cement to withstand Class 3 condition (unless the site investigation report proves that sulphate attack from soils and groundwater will not occur).
 - All opening notices etc. as required under Highways Acts etc. are to be obtained prior to commencement of works. All works are to be inspected by L.A., NHBC or the Network Operator as applicable.
 - Where "Ultra Rib" UPVC pipes (or similar approved) are used in adoptable drainage they shall be handled and laid in accordance with the manufacturers instructions and will be subject to post installation deformation testing prior to adoption. A Class S Bed and Surround must be used for "Ultra Rib" pipes.
 - Trench backfill in highways to within 1m of highway shall, as directed by the Highway Authority be a suitable granular material all in accordance with Sewers for Adoption.
 - Slab levels shall not be varied without reference to the Engineer for guidance.
 - Pipes have not been designed to accommodate construction traffic loading. The contractor is responsible for providing adequate protection to the pipes during construction.



- Legend**
- Proposed
 - S01 Adoptable Surface Water Sewer
 - F01 Adoptable Foul Sewer
 - F101 Private Lateral
 - G Highway Gully
 - Sewer Easement

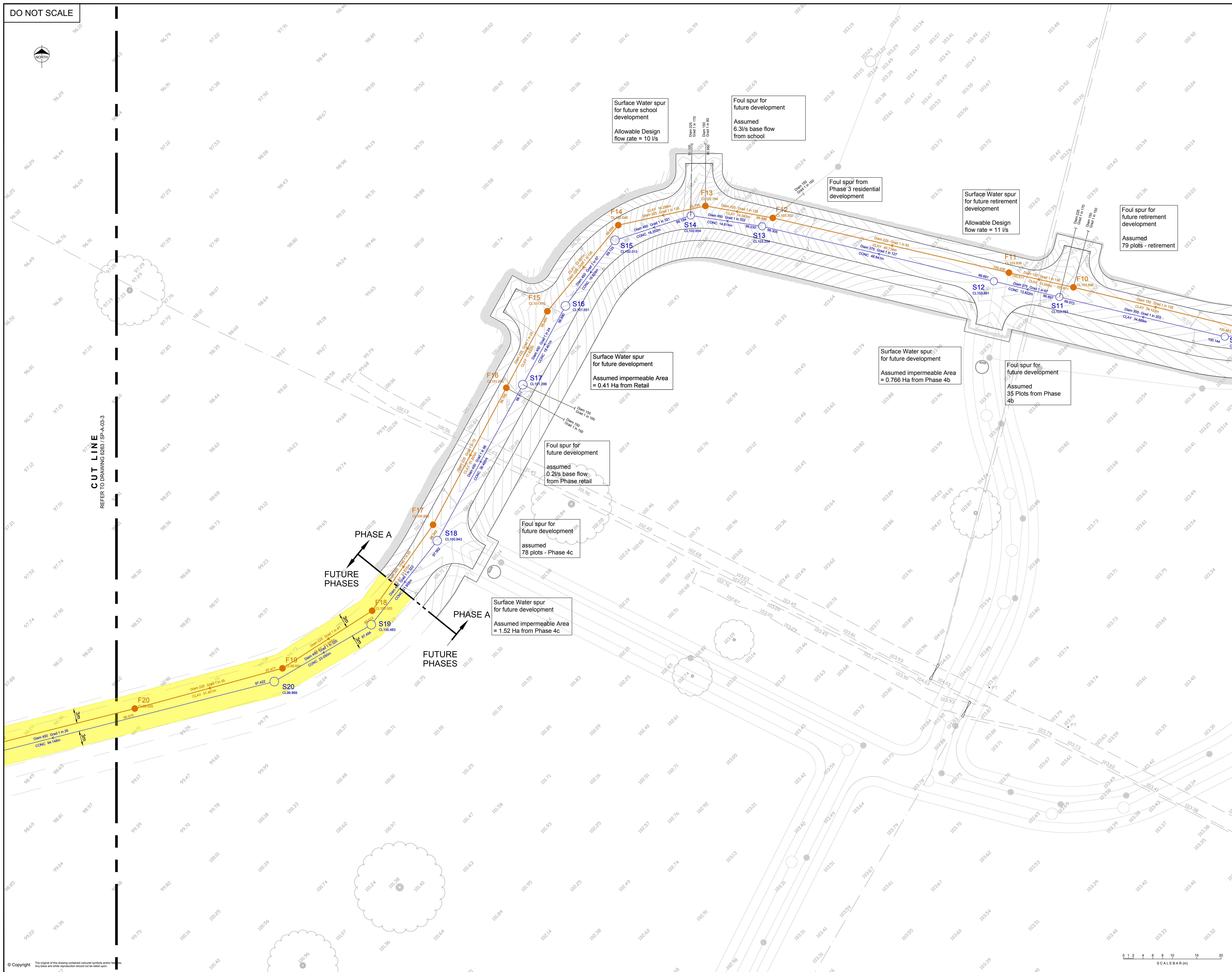
APPROVAL

	30.07.21	Highway extended to site boundary	PJN	AJ
Rev.	Date	Revision	By	Appd.
 coopers chartered consulting engineers				
Tel: 01244 684910 Email: admin@coopers.co.uk Web: http://coopers.co.uk			Park House Sandspur Court Chester Business Park Chester CH4 9QU	
Client Taylor Wimpey				
Project STANDEN HALL CLITHEROE				
Title Spine Road Phase A (Phase 2-4) Drainage Layout Sheet 1 of 4				
DRAWING NUMBER		SCALE at AO		1:250
6263 / SP-A-03-1		DATE		31.03.21
		DRAWN		PJN
		CHECKED		AJ
				REVISION
				A

DO NOT SCALE

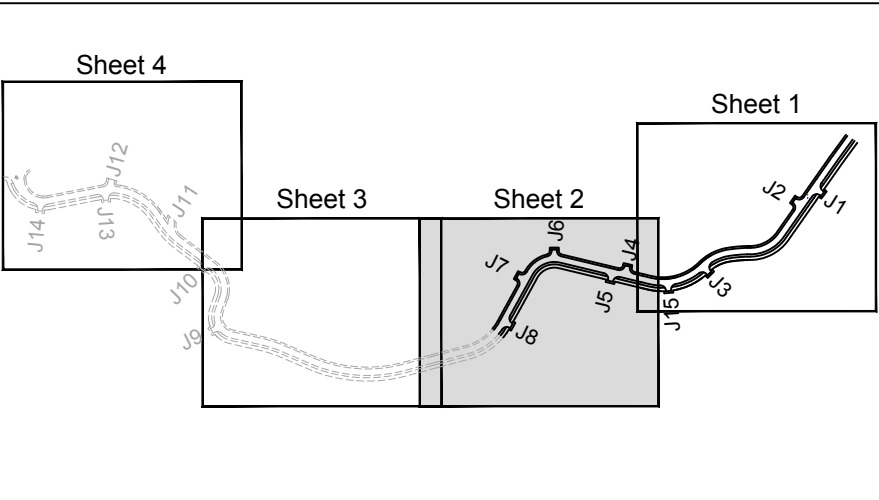


CUT LINE
REFER TO DRAWING 6263 / SP-A-03-3



Notes

- Setting out shall be undertaken using only the information given. Distances should not be scaled from this drawing.
- All sewers shall be constructed in accordance with Sewers for Adoption 6th Edition and United Utilities Details & Guidelines.
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- Slab levels shall not be varied without reference to the Engineer for guidance.
- Pipes have not been designed to accommodate construction traffic loading. The contractor is responsible for providing adequate protection to the pipes during construction.



KEY PLAN

Legend

- Proposed
- S01 Adoptable Surface Water Sewer
 - F01 Adoptable Foul Sewer
 - F101 Private Lateral
 - G Highway Gully
 - Sewer Easement

APPROVAL

Rev	Date	Revision	By	Appd.
A	28.07.21	School, Retirement, Phase 3 parcels notes updated	AJ	AJ

coopers
chartered consulting engineers

Tel: 01244 684910
Email: admin@coopers.co.uk
Web: http://coopers.co.uk

Client: **Taylor Wimpey**

Project: **STANDEN HALL CLITHEROE**

Title: **Spine Road Phase A (Phase 2-4)
Drainage Layout
Sheet 2 of 4**

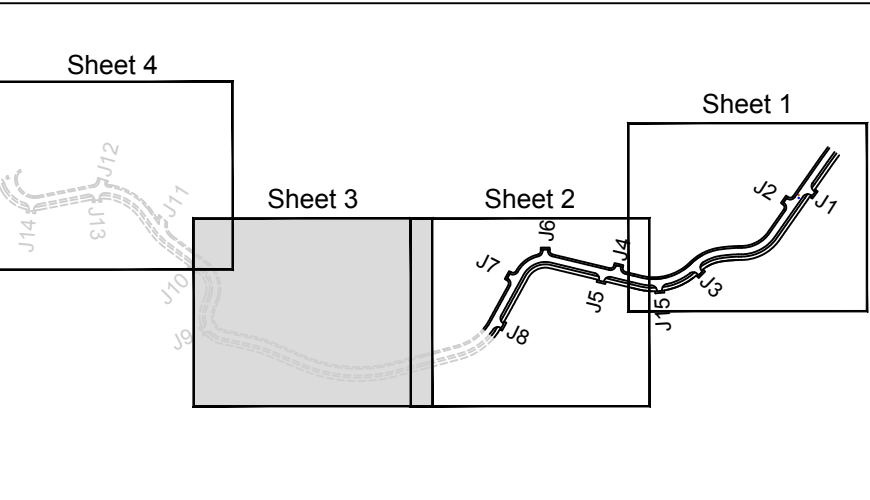
DRAWING NUMBER	SCALE at A0	1:250	DATE	31.03.21	REVISION
6263 / SP-A-03-2	DRAWN	PJN	CHECKED	AJ	A

DO NOT SCALE

CUT LINE
REFER TO DRAWING 6263 / SPA-03-4

Notes

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KEY PLAN

Legend

Proposed

- S01 Adoptable Surface Water Sewer
- F01 Adoptable Foul Sewer
- F101 Private Lateral
- G Highway Gully
- Sewer Easement

APPROVAL

Rev. Date Revision By Appd.
coopers
chartered consulting engineers

Park House
Sandpiper Court
Chester Business Park
Chester
CH4 9QL

Client
Taylor Wimpey

Project
STANDEN HALL CLITHEROE

Title
**Spine Road Phase A (Phase 2-4)
Drainage Layout
Sheet 3 of 4**

DRAWING NUMBER
6263 / SP-A-03-3

SCALE AT A0 1:250
DATE 31.03.21
DRAWN PJN
CHECKED AJ
REVISION -

DO NOT SCALE

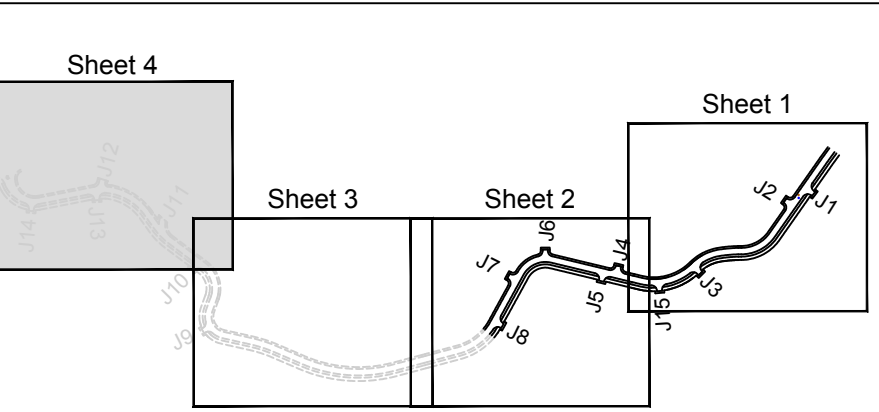


0 1 2 3 4 5 6 7 8 9 10 15 20
SCALE BAR (m)

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Notes

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KEY PLAN

Legend

Proposed

- S01 Adoptable Surface Water Sewer
- F01 Adoptable Foul Sewer
- F101 Private Lateral
- Highway Gully
- Sewer Easement

APPROVAL

Rev.	Date	Revision	By	Appd.
------	------	----------	----	-------

coopers
chartered consulting engineers

Tel: 01244 684910
Email: admin@coopers.co.uk
Web: http://coopers.co.uk

Park House
Sandpiper Court
Chester Business Park
Chester
CH4 5QL

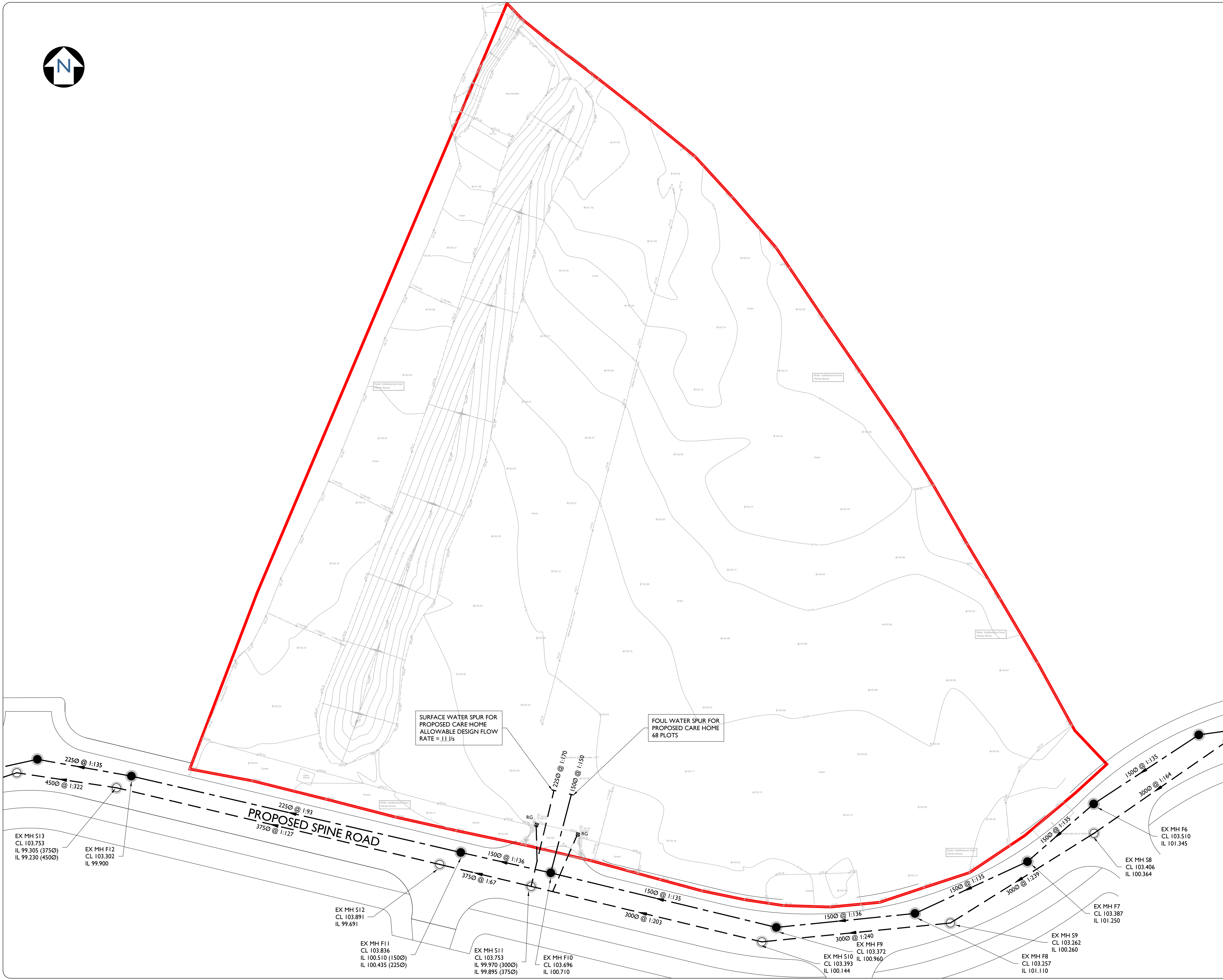
Taylor Wimpey

Project
**STANDEN HALL
CLITHEROE**

Title
**Spine Road Phase A (Phase 2-4)
Drainage Layout
Sheet 4 of 4**

DRAWING NUMBER	SCALE at A0	1:250	DATE	31.03.21	REVISION
6263 / SP-A-03-4	DRAWN	PJN	CHECKED	AJ	-

Appendix G – Existing Drainage Plan



EXISTING DRAINAGE NOTES

THE LOCATION LINE & LEVEL OF ALL KNOWN EXISTING DRAINAGE PIPEWORK INDICATED ON THIS DRAWING IS APPROXIMATE AND FOR GUIDANCE PURPOSES ONLY.

IT IS THE CONTRACTORS RESPONSIBILITY TO DETERMINE THEIR EXACT LINE AND LEVEL BY WAY OF HAND EXCAVATED TRIAL PITS. PRIOR TO THE COMMENCEMENT OF ANY EXCAVATION WORKS ON SITE. THE CONTRACTOR SHALL TAKE ALL NECESSARY PRECAUTIONS AND MAINTAIN THE STRUCTURAL INTEGRITY OF ALL ABOVE AND BELOW GROUND SERVICE INSTALLATIONS.

KEY

- EXISTING FOUL WATER DRAIN
- EXISTING SW DRAIN
- EXISTING ROAD GULLY

NOTE
THE EXISTING DRAINAGE AND CONNECTIONS AS SHOWN HAVE BEEN TAKEN FROM A NUMBER OF SOURCES INCLUDING COOPERS CHARTERED CONSULTING ENGINEERS DRAWINGS 6263 / SP-A-03-1 (30.07.21) REV A - 6263 / SP-A-03-2 (28.07.21) REV A AND SITE SURVEY UNDERTAKEN BY ERIC WRIGHT CONSTRUCTION LTD AND WILL NEED TO BE VERIFIED.

REV	DESCRIPTION	BY	CHK	APR	DATE
-	-	-	-	-	-

+44 (0)1244 893430 | www.jpstructural.co.uk | info@jpstructural.co.uk

PURPOSE OF ISSUE		STATUS
STAGE 2		S2
PROJECT		
CLITHEROE CARE HOME		
TITLE		
DRAINAGE SCHEME EXISTING LAYOUT		
CLIENT		
ERIC WRIGHT CONSTRUCTION LTD		
DRAWN BY	CHECKED BY	APPROVED BY
JR	RH	MM
DATE	SCALE (@ A1)	PROJECT NUMBER
08.02.2023	1:250	113001
DRAWING NUMBER		REV
220018-JPS-ZZ-ZZ-DR-C-00501		P01

Appendix H – Proposed Drainage Layout



NOTE
THE EXISTING DRAINAGE AND CONNECTIONS AS SHOWN HAVE BEEN TAKEN FROM A NUMBER OF SOURCES INCLUDING COOPERS CHARTERED CONSULTING ENGINEERS DRAWINGS 6263 / SP-A-03-1 (30.07.21) REV A - 6263 / SP-A-03-2 (28.07.21) REV A AND SITE SURVEY UNDERTAKEN BY ERIC WRIGHT CONSTRUCTION LTD AND WILL NEED TO BE VERIFIED.

NOTES

1. THE WORKS SHALL BE IN ACCORDANCE WITH THE FOLLOWING SPECIFICATIONS, NATIONAL BUILDING SPECIFICATION (NBS) AND SEWERS FOR ADOPTION, 7TH EDITION.
2. THIS DRAWING IS TO BE READ IN CONJUNCTION WITH ALL RELEVANT ENGINEERS DRAWINGS, ARCHITECTS DRAWINGS, MECHANICAL AND ELECTRICAL DRAWINGS AND SPECIFICATIONS.
3. THE LOCATION, LINE & LEVEL OF ALL KNOWN EXISTING BURIED SERVICE MAINS AND DRAINAGE PIPEWORK INDICATED ON THE DRAWINGS ARE APPROXIMATE AND FOR GUIDANCE PURPOSES ONLY. IT IS THE CONTRACTOR'S RESPONSIBILITY TO DETERMINE THEIR EXACT LINE & LEVEL, BY WAY OF HAND EXCAVATED TRIAL PITS, PRIOR TO THE COMMENCEMENT OF ANY EXCAVATION WORKS ON SITE. THE CONTRACTOR SHALL TAKE ALL NECESSARY PRECAUTIONS TO MAINTAIN THE STRUCTURAL INTEGRITY OF ALL ABOVE AND BELOW GROUND SERVICE MAINS / DRAINAGE INSTALLATIONS.
4. THE CONTRACTOR MUST COMPLY WITH ALL CURRENT LEGISLATION RELATING TO HEALTH & SAFETY.
5. THE MAIN CONTRACTOR IS RESPONSIBLE FOR THE DESIGN OF ALL TEMPORARY WORKS, AND IS ALSO RESPONSIBLE FOR THE SAFE MAINTENANCE AND STABILITY OF EXISTING BUILDINGS AT ALL TIMES.
6. THE MAIN CONTRACTOR IS RESPONSIBLE FOR THE MITIGATION OF ALL OCCURRENCES OF GROUND WATER DURING THE CONSTRUCTION PERIOD.
7. THE CONTRACTOR SHALL MAKE ALLOWANCE FOR RAISING / LOWERING ALL EXISTING ACCESS COVERS & FRAMES TO SUIT NEW FINISHED LEVELS.
8. ALL SOFT / HARD PAVED AREAS AFFECTED BY THE WORKS SHALL BE FULLY REINSTATED UPON COMPLETION OF THE WORKS. ALL SURFACE MARKINGS DAMAGED BY THE WORKS SHALL BE FULLY REINSTATED.
9. ALL SURPLUS EXCAVATED MATERIAL SHALL BE DISPOSED OF OFF SITE.
10. ALL LEVELS ARE TO ORDNANCE DATUM

KEY

- EXISTING FOUL WATER DRAIN
- EXISTING SW DRAIN
- PROPOSED FOUL SEWER
- PROPOSED SW SEWER
- PROPOSED ATTENUATION CRATES
- LINEAR DRAINAGE CHANNEL CHANNEL (SU - UNIVERSAL SUMP UNIT WITH AIR TRAP)
- PROPOSED TRAPPED ROAD GULLY (1500 OUTLET)
- PROPOSED RAIN WATER DOWN PIPE (1000 OUTLET)
- PROPOSED FOUL OUTLET (1500 OUTLET)

ATTENUATION TANK
301m³ OF ATTENUATION CONSISTING OF AQUACELL 'CORE-R' GEOCELLULAR BLOCKS - 44 UNITS x 9 UNITS x 4 UNITS (22.0m x 9.0m x 1.6m AT 95% VOID RATIO) TO BE INSTALLED IN ACCORDANCE WITH MANUFACTURER'S GUIDANCE & RECOMMENDATIONS CL 102.500 TOP 101.900
1 YEAR CRITICAL WATER LEVEL 100.528m AOD
2 YEAR CRITICAL WATER LEVEL 100.606m AOD
30 YEAR CRITICAL WATER LEVEL 101.036m AOD
100 YEAR +50%CC CRITICAL WATER LEVEL 101.901m AOD

P04	SW AMENDED FOLLOWING LLFA COMMENTS	JR	RH	MM	14.06.2023
P03	ISSUED FOR TENDER	JR	RH	MM	16.05.2023
P02	SITE LAYOUT AMENDED	JR	RH	MM	27.03.2023
REV	DESCRIPTION	BY	CHK	APR	DATE



PURPOSE OF ISSUE	FOR TENDER	STATUS	D2
PROJECT	CLITHEROE CARE HOME		
TITLE	DRAINAGE SCHEME PROPOSED LAYOUT		
CLIENT	ERIC WRIGHT CONSTRUCTION LTD		
DRAWN BY	JR	CHECKED BY	RH
DATE	08.02.2023	SCALE (@ A1)	1:250
DRAWING NUMBER	220018-JPS-ZZ-ZZ-DR-C-00502	APPROVED BY	MM
		PROJECT NUMBER	113001
		REV	P04

Appendix I – Proposed Drainage Calculations

Simulation Settings

Rainfall Methodology	FSR	Analysis Speed	Normal
FSR Region	England and Wales	Skip Steady State	x
M5-60 (mm)	20.000	Drain Down Time (mins)	240
Ratio-R	0.300	Additional Storage (m ³ /ha)	0.0
Summer CV	0.750	Check Discharge Rate(s)	x
Winter CV	0.840	Check Discharge Volume	x

Storm Durations

15 | 30 | 60 | 120 | 180 | 240 | 360 | 480 | 600 | 720 | 960 | 1440

Return Period (years)	Climate Change (CC %)	Additional Area (A %)	Additional Flow (Q %)
1	0	0	0
2	0	0	0
30	0	0	0
100	50	0	0

Node 1.5 Online Hydro-Brake® Control

Flap Valve	x	Objective	(HE) Minimise upstream storage
Downstream Link	1.005	Sump Available	✓
Replaces Downstream Link	✓	Product Number	CTL-SHE-0094-6000-2700-6000
Invert Level (m)	100.200	Min Outlet Diameter (m)	0.150
Design Depth (m)	2.700	Min Node Diameter (mm)	1200
Design Flow (l/s)	6.0		

Node TANK Depth/Area Storage Structure

Base Inf Coefficient (m/hr)	0.00000	Safety Factor	2.0	Invert Level (m)	100.300
Side Inf Coefficient (m/hr)	0.00000	Porosity	0.95	Time to half empty (mins)	

Depth (m)	Area (m ²)	Inf Area (m ²)	Depth (m)	Area (m ²)	Inf Area (m ²)	Depth (m)	Area (m ²)	Inf Area (m ²)
0.000	198.0	0.0	1.600	198.0	0.0	1.601	0.0	0.0

Results for 1 year Critical Storm Duration. Lowest mass balance: 95.28%

Node Event	US Node	Peak (mins)	Level (m)	Depth (m)	Inflow (l/s)	Node Vol (m³)	Flood (m³)	Status
15 minute winter	3.0	10	102.235	0.035	3.1	0.0056	0.0000	OK
15 minute winter	3.1	11	101.918	0.058	8.0	0.0164	0.0000	OK
15 minute winter	3.2	11	101.383	0.078	12.1	0.0222	0.0000	OK
15 minute winter	3.3	10	101.151	0.051	17.5	0.0143	0.0000	OK
240 minute winter	3.4	184	100.528	0.237	8.8	0.4196	0.0000	OK
240 minute winter	1.5	184	100.527	0.327	8.8	0.5785	0.0000	SURCHARGED
15 minute summer	1.6	1	100.130	0.000	4.2	0.0000	0.0000	OK
15 minute winter	4.0	10	102.245	0.045	5.8	0.0071	0.0000	OK
15 minute winter	5.0	10	100.642	0.042	5.3	0.0470	0.0000	OK
240 minute winter	5.1	184	100.528	0.217	2.7	0.3843	0.0000	OK
240 minute winter	TANK	184	100.528	0.227	10.9	42.7918	0.0000	OK
15 minute winter	2.1	10	101.136	0.036	5.6	0.0103	0.0000	OK
15 minute winter	2.0	10	102.245	0.045	5.8	0.0071	0.0000	OK
15 minute winter	1.0	10	101.419	0.069	8.5	0.0775	0.0000	OK
15 minute winter	1.1	11	101.342	0.102	19.3	0.1158	0.0000	OK
15 minute winter	1.2	11	101.094	0.124	24.4	0.1404	0.0000	OK
15 minute winter	1.3	11	100.999	0.124	25.5	0.1402	0.0000	OK
15 minute winter	1.4	11	100.858	0.068	30.8	0.0767	0.0000	OK
Link Event (Upstream Depth)	US Node	Link	DS Node	Outflow (l/s)	Velocity (m/s)	Flow/Cap	Link Vol (m³)	Discharge Vol (m³)
15 minute winter	3.0	3.000	3.1	3.1	1.004	0.112	0.0343	
15 minute winter	3.1	3.001	3.2	7.7	0.771	0.148	0.5623	
15 minute winter	3.2	3.002	3.3	11.9	1.272	0.227	0.1908	
15 minute winter	3.3	3.003	3.4	17.5	2.436	0.107	0.0588	
240 minute winter	3.4	3.004	1.5	-4.3	0.225	-0.060	1.3615	
240 minute winter	1.5	Hydro-Brake®	1.6	4.3				89.6
15 minute winter	4.0	4.000	3.3	5.6	1.291	0.188	0.1585	
15 minute winter	5.0	5.000	5.1	5.2	0.645	0.042	0.2818	
240 minute winter	5.1	5.001	TANK	2.4	0.913	0.022	0.0560	
240 minute winter	TANK	5.002	3.4	-8.5	-0.634	-0.077	0.0586	
15 minute winter	2.1	2.001	1.4	5.6	1.419	0.049	0.0198	
15 minute winter	2.0	2.000	2.1	5.6	1.291	0.188	0.1585	
15 minute winter	1.0	1.000	1.1	8.3	0.510	0.117	0.4383	
15 minute winter	1.1	1.001	1.2	18.8	0.783	0.256	1.4994	
15 minute winter	1.2	1.002	1.3	24.1	0.879	0.325	0.5800	
15 minute winter	1.3	1.003	1.4	25.2	1.312	0.340	0.3723	
15 minute winter	1.4	1.004	1.5	30.7	0.730	0.113	0.4023	

Results for 2 year Critical Storm Duration. Lowest mass balance: 95.28%

Node Event	US Node	Peak (mins)	Level (m)	Depth (m)	Inflow (l/s)	Node Vol (m³)	Flood (m³)	Status
15 minute winter	3.0	10	102.240	0.040	4.0	0.0063	0.0000	OK
15 minute winter	3.1	10	101.926	0.066	10.2	0.0187	0.0000	OK
15 minute winter	3.2	11	101.395	0.090	15.5	0.0255	0.0000	OK
15 minute winter	3.3	10	101.156	0.056	22.5	0.0160	0.0000	OK
240 minute winter	3.4	184	100.613	0.323	11.5	0.5708	0.0000	SURCHARGED
240 minute winter	1.5	196	100.609	0.409	10.7	0.7225	0.0000	SURCHARGED
15 minute summer	1.6	1	100.130	0.000	4.3	0.0000	0.0000	OK
15 minute winter	4.0	10	102.251	0.051	7.5	0.0082	0.0000	OK
15 minute winter	5.0	10	100.647	0.047	6.8	0.0531	0.0000	OK
240 minute winter	5.1	184	100.607	0.297	3.3	0.5247	0.0000	OK
240 minute winter	TANK	188	100.606	0.306	14.0	57.5612	0.0000	SURCHARGED
15 minute winter	2.1	10	101.142	0.042	7.3	0.0118	0.0000	OK
15 minute winter	2.0	10	102.251	0.051	7.5	0.0082	0.0000	OK
15 minute winter	1.0	10	101.428	0.078	10.9	0.0879	0.0000	OK
15 minute winter	1.1	11	101.357	0.117	25.0	0.1327	0.0000	OK
15 minute winter	1.2	11	101.115	0.145	31.5	0.1637	0.0000	OK
15 minute winter	1.3	11	101.018	0.143	33.3	0.1615	0.0000	OK
15 minute winter	1.4	11	100.868	0.078	40.2	0.0877	0.0000	OK
Link Event (Upstream Depth)	US Node	Link	DS Node	Outflow (l/s)	Velocity (m/s)	Flow/Cap	Link Vol (m³)	Discharge Vol (m³)
15 minute winter	3.0	3.000	3.1	3.9	1.077	0.144	0.0412	
15 minute winter	3.1	3.001	3.2	9.9	0.824	0.190	0.6755	
15 minute winter	3.2	3.002	3.3	15.3	1.375	0.293	0.2272	
15 minute winter	3.3	3.003	3.4	22.6	2.423	0.137	0.0793	
240 minute winter	3.4	3.004	1.5	-6.1	0.234	-0.083	1.4723	
240 minute winter	1.5	Hydro-Brake®	1.6	4.4				106.7
15 minute winter	4.0	4.000	3.3	7.3	1.387	0.244	0.1915	
15 minute winter	5.0	5.000	5.1	6.7	0.693	0.054	0.4211	
240 minute winter	5.1	5.001	TANK	2.9	1.001	0.026	0.0703	
240 minute winter	TANK	5.002	3.4	-11.1	-0.602	-0.100	0.0704	
15 minute winter	2.1	2.001	1.4	7.2	1.520	0.064	0.0240	
15 minute winter	2.0	2.000	2.1	7.3	1.387	0.244	0.1915	
15 minute winter	1.0	1.000	1.1	10.7	0.544	0.150	0.5263	
15 minute winter	1.1	1.001	1.2	24.3	0.834	0.331	1.8212	
15 minute winter	1.2	1.002	1.3	31.4	0.940	0.422	0.7036	
15 minute winter	1.3	1.003	1.4	33.0	1.413	0.444	0.4486	
15 minute winter	1.4	1.004	1.5	40.1	0.827	0.148	0.4262	

Results for 30 year Critical Storm Duration. Lowest mass balance: 95.28%

Node Event	US Node	Peak (mins)	Level (m)	Depth (m)	Inflow (l/s)	Node Vol (m³)	Flood (m³)	Status
15 minute winter	3.0	10	102.256	0.056	7.5	0.0089	0.0000	OK
15 minute winter	3.1	10	101.953	0.093	19.3	0.0263	0.0000	OK
15 minute winter	3.2	11	101.435	0.130	29.6	0.0369	0.0000	OK
15 minute winter	3.3	10	101.178	0.078	42.7	0.0221	0.0000	OK
360 minute winter	3.4	304	101.074	0.784	17.4	1.3859	0.0000	SURCHARGED
360 minute winter	1.5	352	101.036	0.836	14.5	1.4764	0.0000	SURCHARGED
15 minute summer	1.6	1	100.130	0.000	4.4	0.0000	0.0000	OK
15 minute winter	4.0	10	102.273	0.073	14.1	0.0117	0.0000	OK
360 minute winter	5.0	352	101.039	0.439	2.2	0.4967	0.0000	SURCHARGED
360 minute winter	5.1	352	101.040	0.730	4.3	1.2901	0.0000	SURCHARGED
360 minute winter	TANK	344	101.036	0.736	22.9	138.4166	0.0000	SURCHARGED
15 minute winter	2.1	10	101.159	0.059	13.8	0.0167	0.0000	OK
15 minute winter	2.0	10	102.273	0.073	14.1	0.0117	0.0000	OK
15 minute winter	1.0	10	101.459	0.108	20.7	0.1227	0.0000	OK
15 minute winter	1.1	11	101.410	0.170	47.4	0.1921	0.0000	OK
15 minute winter	1.2	11	101.193	0.223	60.3	0.2524	0.0000	OK
15 minute winter	1.3	11	101.082	0.207	63.3	0.2339	0.0000	OK
360 minute winter	1.4	352	101.035	0.245	13.5	0.2775	0.0000	OK
Link Event (Upstream Depth)	US Node	Link	DS Node	Outflow (l/s)	Velocity (m/s)	Flow/Cap	Link Vol (m³)	Discharge Vol (m³)
15 minute winter	3.0	3.000	3.1	7.4	1.276	0.272	0.0657	
15 minute winter	3.1	3.001	3.2	18.9	0.969	0.363	1.0802	
15 minute winter	3.2	3.002	3.3	29.2	1.626	0.557	0.3631	
15 minute winter	3.3	3.003	3.4	42.8	2.502	0.260	0.1814	
360 minute winter	3.4	3.004	1.5	-10.0	0.144	-0.137	1.4723	
360 minute winter	1.5	Hydro-Brake®	1.6	4.4				134.7
15 minute winter	4.0	4.000	3.3	13.8	1.639	0.461	0.3069	
360 minute winter	5.0	5.000	5.1	2.1	0.296	0.017	1.6246	
360 minute winter	5.1	5.001	TANK	6.5	0.977	0.058	0.0704	
360 minute winter	TANK	5.002	3.4	-16.4	-0.362	-0.147	0.0704	
15 minute winter	2.1	2.001	1.4	13.7	1.791	0.122	0.0387	
15 minute winter	2.0	2.000	2.1	13.8	1.639	0.461	0.3069	
15 minute winter	1.0	1.000	1.1	20.4	0.639	0.286	0.8475	
15 minute winter	1.1	1.001	1.2	46.1	0.963	0.629	2.9964	
15 minute winter	1.2	1.002	1.3	59.8	1.107	0.805	1.1395	
15 minute winter	1.3	1.003	1.4	63.2	1.637	0.851	0.7336	
360 minute winter	1.4	1.004	1.5	13.5	0.310	0.050	0.6638	

Results for 100 year +50% CC Critical Storm Duration. Lowest mass balance: 95.28%

Node Event	US Node	Peak (mins)	Level (m)	Depth (m)	Inflow (l/s)	Node Vol (m³)	Flood (m³)	Status
15 minute winter	3.0	10	102.284	0.084	14.6	0.0133	0.0000	OK
15 minute winter	3.1	10	101.999	0.138	37.6	0.0392	0.0000	OK
360 minute winter	3.2	344	101.904	0.599	9.9	0.1695	0.0000	SURCHARGED
360 minute winter	3.3	352	101.903	0.803	14.6	0.2272	0.0000	SURCHARGED
480 minute winter	3.4	408	101.907	1.617	27.1	2.8573	0.0000	SURCHARGED
600 minute winter	1.5	495	101.902	1.702	17.1	3.0071	0.0000	SURCHARGED
15 minute summer	1.6	1	100.130	0.000	4.4	0.0000	0.0000	OK
15 minute winter	4.0	10	102.316	0.116	27.4	0.0185	0.0000	OK
480 minute winter	5.0	392	101.905	1.305	3.4	1.4762	0.0000	SURCHARGED
720 minute winter	5.1	570	101.908	1.598	4.9	2.8244	0.0000	SURCHARGED
600 minute winter	TANK	570	101.901	1.601	27.1	301.0473	0.0000	SURCHARGED
600 minute winter	2.1	495	101.904	0.803	3.2	0.2274	0.0000	SURCHARGED
15 minute winter	2.0	10	102.316	0.116	27.4	0.0185	0.0000	OK
15 minute winter	1.0	12	102.270	0.920	40.2	1.0405	0.0000	SURCHARGED
15 minute winter	1.1	12	102.240	1.000	84.2	1.1306	0.0000	SURCHARGED
15 minute winter	1.2	12	101.911	0.941	106.7	1.0642	0.0000	SURCHARGED
600 minute winter	1.3	495	101.903	1.028	13.9	1.1628	0.0000	SURCHARGED
600 minute winter	1.4	495	101.903	1.113	16.0	1.2586	0.0000	SURCHARGED
Link Event (Upstream Depth)	US Node	Link	DS Node	Outflow (l/s)	Velocity (m/s)	Flow/Cap	Link Vol (m³)	Discharge Vol (m³)
15 minute winter	3.0	3.000	3.1	14.5	1.499	0.529	0.1089	
15 minute winter	3.1	3.001	3.2	37.0	1.112	0.709	1.7929	
360 minute winter	3.2	3.002	3.3	10.0	1.207	0.192	0.8020	
360 minute winter	3.3	3.003	3.4	14.0	1.523	0.085	0.2948	
480 minute winter	3.4	3.004	1.5	-15.6	-0.222	-0.215	1.4723	
600 minute winter	1.5	Hydro-Brake®	1.6	4.8				214.0
15 minute winter	4.0	4.000	3.3	26.8	1.878	0.894	0.5203	
480 minute winter	5.0	5.000	5.1	3.5	0.337	0.028	1.6246	
720 minute winter	5.1	5.001	TANK	8.5	0.941	0.076	0.0704	
600 minute winter	TANK	5.002	3.4	-21.6	-0.437	-0.195	0.0704	
600 minute winter	2.1	2.001	1.4	3.0	1.157	0.027	0.2002	
15 minute winter	2.0	2.000	2.1	26.8	1.873	0.894	0.5694	
15 minute winter	1.0	1.000	1.1	34.9	0.677	0.489	1.8653	
15 minute winter	1.1	1.001	1.2	80.3	1.140	1.095	4.3352	
15 minute winter	1.2	1.002	1.3	103.3	1.468	1.391	1.4858	
600 minute winter	1.3	1.003	1.4	13.4	1.029	0.181	1.3316	
600 minute winter	1.4	1.004	1.5	15.8	0.297	0.058	0.7076	