Former private garages site at Princess Avenue Clitheroe

Proposed housing

Flood Risk Assessment

NGR SD 746 423

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1.0 Introduction

Four apartments are proposed for a former private garages site between 15 and 17 Princess Avenue, Clitheroe. This report covers the flood risk and surface water aspects of the proposal.

2.0 Executive summary

Four apartments are proposed for a former lockup garage site. The site is floodzone 2 on the Environment Agency floodrisk zone maps. Detailed hydraulic river modelling shows that risk levels are lower and the site is in practice floodzone 1. The proposal is suitable for the residential area, surface water discharges to the beck will reduce in terms of flow rates and volumes and flood risk to others will decrease. New hard area will be less than before and SR744 is complied with.

3.0 Existing site and river system.

The existing site is a block of former rented private garages with an access from Princess Avenue between house numbers 15 and 17. The site has been surveyed and has a level range of 76.86 to 77.3. There is a concrete slab yard area in front of the garages which slopes towards the stream and runoff from the overall hard area of approx 200m2 will flow straight into the stream. Chatburn Beck (Pimlico watercourse) flows through the site in open channel. The Beck flows under Princess Avenue in culvert and also flows into a culvert approx 40m downstream of the site. To the west of the site the gardens and private ground to Well Court slope away to a lower level.

The upstream beck catchment has a catchment area of 1.61 km2. Annual rainfall is 1222mm, average bedslope DPSBAR is 40.3 m/km indicating a flattish catchment and SPRHOST is 30.24%. The catchment is thin with a length to width average ratio of 2.

4.0 Hydrology and river modelling

WinFAP3 software has been utilised to find similar catchments. A pooling group analysis was then carried out resulting in a Q100 flow of 4 m3/sec. This is approx 2.5 times the area and based on our own in house data from the analysis of over 200 small catchments is the sort of figure we would expect. To uprate the Q100 flow to Q1000 a growth factor of 1.7 has been used. Q100 + CC is $4.8 \, \text{m3/sec}$ and Q1000 is $6.8 \, \text{m3/sec}$.

Cross section points have been selected on the site survey and cross section data input to Hec Ras 4.1.0 using survey levels. The river channel consists of vertical brick walls with a natural bed and 'n' values of 0.020 walls and 0.035 bed have been input. As can be seen on Google Earth the land to Well Court is lower and flow can spill over the channel wall towards Well Court. A lateral sideweir has been put into the model at the channel bend to simulate this.

The model has been run for Q100, Q100+ CC, and Q1000 flows. Cross sections 2 to 5 apply to the proposal and risk level results are as follows:-

Q100- flow 0.2m to 0.8m below the channel wall

Q100 + CC- flow 0.15m to 0.25m below the channel wall Q1000- flow level at wall top level to 0.35 below the channel wall

The results show that the site is floodzone 1 above the 1 in 1000 year risk level. We applied to the Environment Agency for risk levels for the beck and the 1 in 1000 year risk levels at the EA nodes 0421 and 0461 are 750mm above existing ground levels which is unlikely to occur in practice as sidespills will occur. We expect that the EA modelling will have cross sections with 'glass walls' at either side of the channel which produce artificially high risk levels.

5.0 Proposals and drainage

The proposals are for the demolition of the garages and the building of four apartments as one building. Drainage will be separate system with surface water draining to the beck and foul draining to Princess Avenue public sewer system via a submersible pumping station.

The guidelines for surface water runoff management for developments (2004 Gibbs paper) have been revised in Jan 2012 and are now contained in SR744 – 'preliminary rainfall runoff management for developments'. They allow comparison of proposals with the existing drainage performance of the site (principle 4) and on this basis surface water runoff rates and volumes will decrease as a result of the proposal and surface water attenuation will not be needed.

The beck is in open channel form between Princess Avenue and Well Court boundary where it goes into culvert. The culvert inlet is a blockage risk point and access is from Well Croft or 2 Causeway Croft rear garden. The beck channel inside the site is brick walls and access to the beck is at present from the access road to the existing garages and will continue to be so if the proposal is consented. The new apartments garden areas and the new building is shown partly within the 8m strip that the EA can ask to be kept clear, however the beck channel access is by climbing down into the channel from the access roadway and we would suggest that the proposal will not compromise maintenance access.

6.0 National Planning Policy Framework and Technical Guidance

The proposals are for housing, and are classed as 'more vulnerable' in Table 2, and are 'appropriate' in floodzone 1 as per Table 3.

All forms of flooding (PPS25 notation) are:-

C4 – rivers – see above

C5 – sea – no tidal influence

C6 – land – no undrained land slopes towards either site

C7 – groundwater – no springs or weep areas on site

C8 – sewers – no reported incidents of on-site sewer flooding

C9 – reservoirs, canals – none nearby

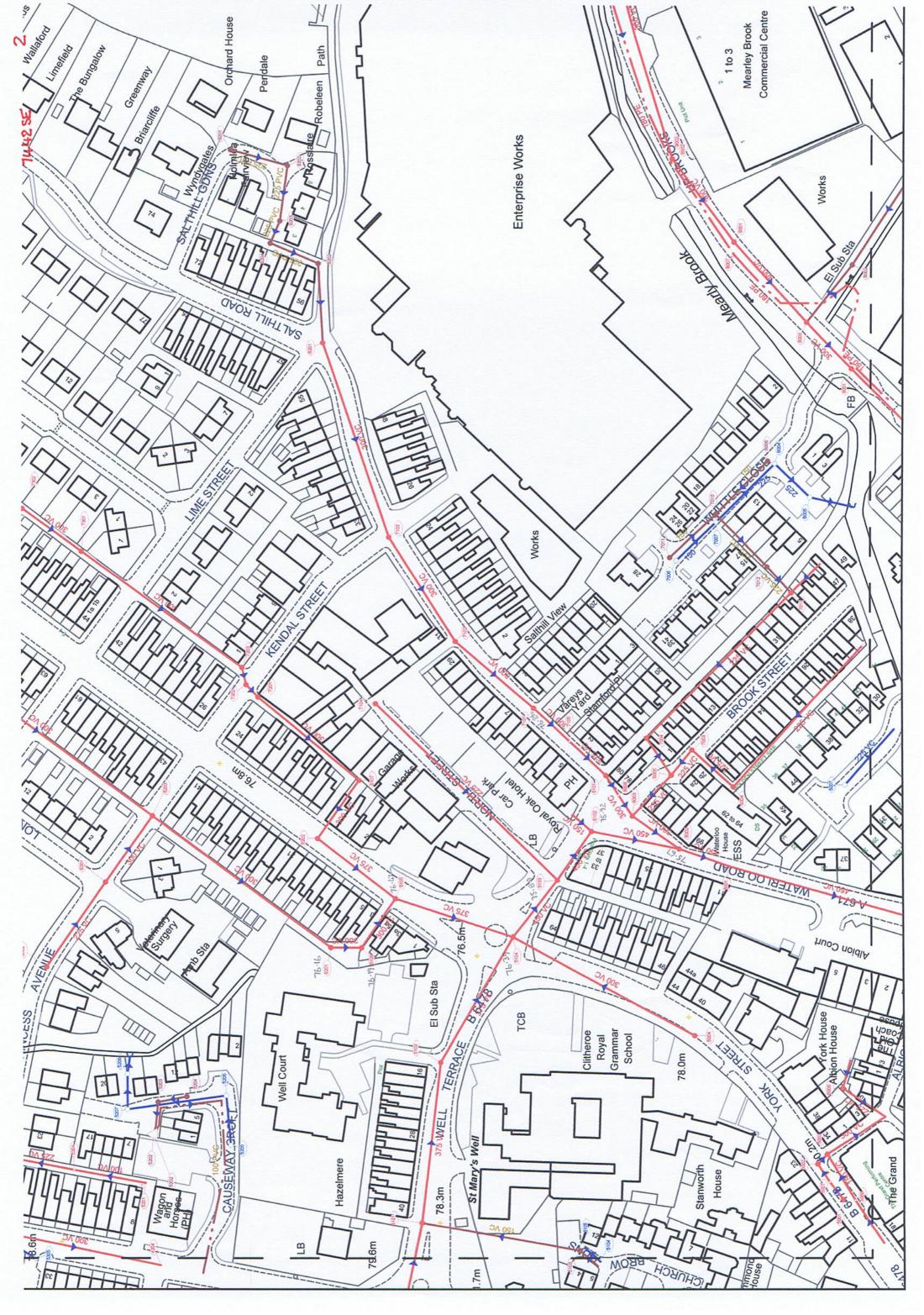
7.0 Attachments

Attachment	number	size
Site location and sewer	1 to 5	A3
records		
Site survey and river cross	6, 7	A3
section positions		
Proposals	8	A3
Environment Agency risk	9, 10	A3
level data		
Hec Ras outputs Q100,	11 to 19	A3
Q100+CC, Q1000		
FEH catchment plan	20	A3
FEH descriptors	21	A4
FEH rain data	22	A4

This report is an email report and A4 and A3 attachments are grouped for scanning and can be put in order by using the top RH corner lettering.

Email file list 130205fra01 130206attach1-A3 130206attach2-A3 130206attach3-A4





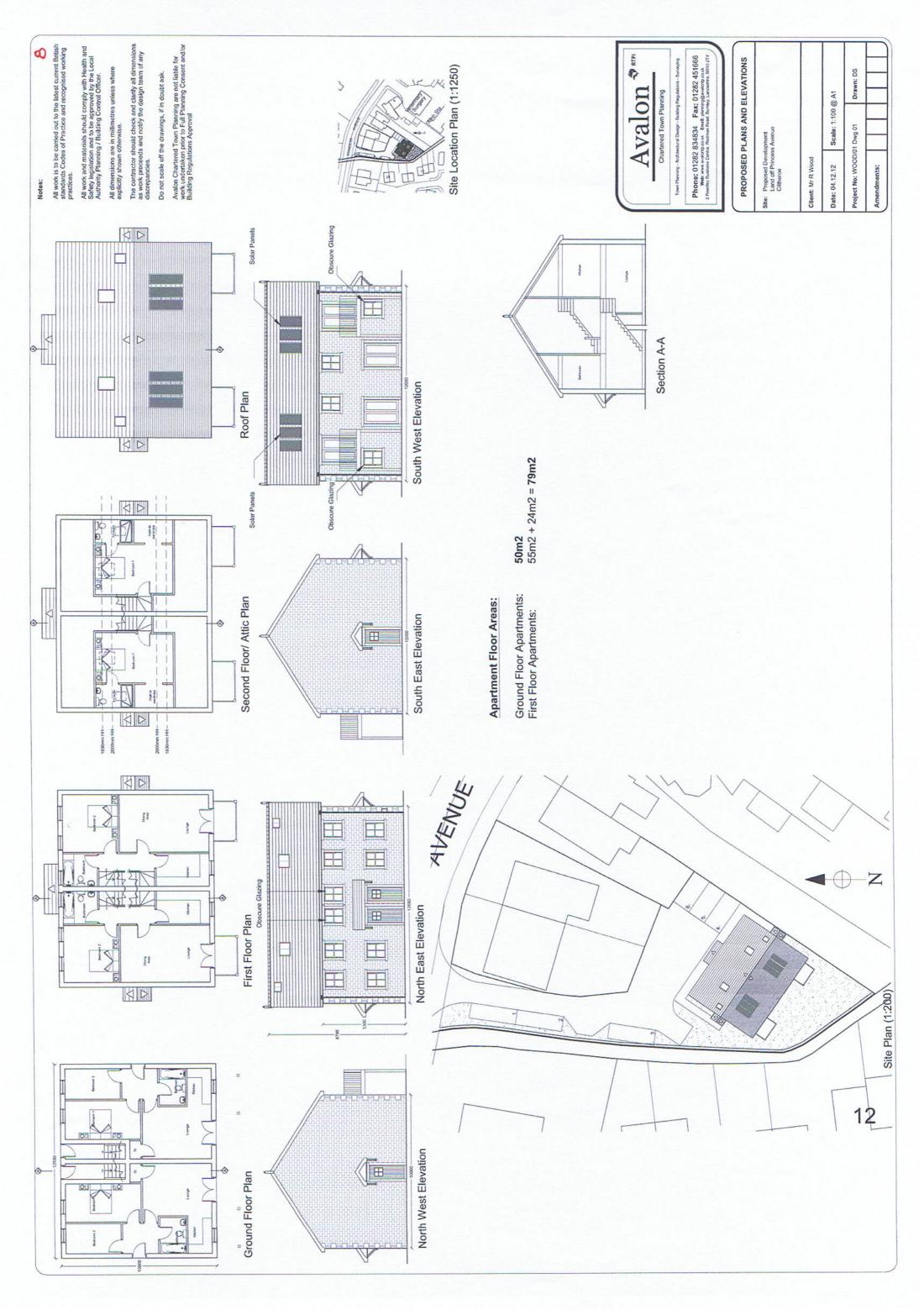
Scale 1:1 **1S SO** 3 Crown Copyright Unauthorised rel with the sanctior This plan is base I N I AM I AM PF I I dd AC TS RP ЬE Λd I Sd GR (OB (1 10 22 I SO SO 1 00 ; IS) 10 88 1 DA **SEMI** S S R Re 13 B 0 0 E E C C! **SEMI** 1T W I a DS S 1d d A CC F Oi צ צי 3H H 27 7 UL L W W INAM כ כי 15 S 거 크 INAM NOE b woft JJA - stoM 48 EJ 74 SURF П CONT IAHO [D CATC UTIB 🛄 EXPEI CHOS INSP INCE. HADI 1A3H 1A3H)TAH CULI **LLOV 3TX3** CON. CON. CASC VAIA ... SITE .

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0916		S	F							7525		F	M		150	С	VC		6.15	327 MINE
5501	74.18	C	M	70.39	900	C	VC		27.55	7527		F	M		150	С	VC		3.65	
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5504		С	L		225	С	VC		18.44	7602	77.35	С	М	74.9	300	С	vc	21	32.32	
5505		С	G		225	C	vc		34.25	7603		F	М						22.51	
5506 5507	75.9	C	L M	73.62	225 225	c	VC	142	19.52 29.82	7604 7605		F	M		300		vc		25.6 7.8	
5508	70.0	C	G	10.02	225		VC	172	45.17	7606		F	М		300		VC		25.04	
5509		C	Q		525	С	VC		28.26	7607		F	М		300		vc		11.51	
5601	75.46	C	M	70.88	900	С	VC	214	100.77	7608		F	M		300		VC		9.63	
5701 5702	75.16 75.14	C	M	72.63	225	C	VC	68	29.4 5.32	7609 7610		c	M		300	С	VC		26.73 25.74	
5801	77.58	C	м	74.99	225	C	VC		55.57	7611		S	M						11.33	
5802	78.16	C	М	76.89	225	С	vc	10	18.75	7612		S	M						8.22	
5803	78.48	C	M	77.08	225	C	VC	204	32.62	7613		F	M						22.35	
5804 5805		C	M		100	C	VC		12.52	7701 7702		F	M		375	С			20.8	
5901	77.62	С	М	75.3	300	С	VC	21	12.82	7703		s	М						29.4	
5902		С	L	74.06	225	С	VC	82	13.9	7704		F	M						32.69	
5903 5904	78.27	C	M	76.1	225 225	C	VC VC		7.02	7801 7901	74.93 75.37	C	M	72.43 72.97	375 300	C	VC	239	45.47 23.51	
5905		C	J		225	C	VC		17.28	7902	75.66	C	M	73.26	300	c	VC	40	11.49	
5906		C	G		300	С	VC		20.49	7903		С	М	72.69	375	С	vc	160	38.42	
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6502	79.97	c	м	77.88	300	c	vc	44	43.1	7907	76.24	s	м	74.33	450	C	co	106	15.92	
6503	79.02	С	М	76.89	300	С	VC	27	51.61	7908	75.86	S	М	74.57	225	С	vc	104	25.07	
6504 6505		C	G		225	С	VC		33.21	7909 7910	75.85	F	M	74.17	150	C	VC		31.48	
6506		C	J							7910	76.2	F	M	74.17	150 150	C	VC	35	18.03	
6507		F	3		150	С	vc		2.65	7912		С	М		300	С	VC		8.42	
6508		F	D		150	C	VC		2.63	7913		C	н	74.48	180	C	PE		149.26	
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6511		F	D		150	c	VC		3.47	8503	86.82	C	М	84.62	300	c	VC	16	79.62	
6512		S	D		150	С	VC		2.26	8504		S	M			C			28.97	
6513		S	J							8505		S	F		450				47.07	
6514 6515		C	M		100	С	vc		2.96	8601 8602		F	M		150 150	C	VC		17.27 29.48	
6516		С	M		100	C	VC		21.81	8603		F	М		150	c			57.98	
6517		C	M		100	С	vc		12.15	8604		F	М						15.52	
6518 6519		C	M		100	С	VC		7.79	8605		S	M		200	С	VC		9.58	
6520		C	J							8606 8607		S	M		300	c	VC		17.63 30.04	
6601	76.19	С	M	73.35	300	С	VC	22	36.54	8608		S	М		150	С	vc		58.67	
6602		С	M	71.27	900	С	VC	263	97.28	8609		S	M						16.22	
6603 6701	75.96 75.09	C	M	73.33	300 825	C	VC	62	26.57 19.17	8610 8611		S	M						29.33 16.1	
6702		C	M		825	c	CO		15.73	8701		F	М		150	С	vc		32.15	
6703		C	M		825	С	co		14.6	8702		F	М						25.71	
6704		C	Q	72.2	300	C	VC	70	29.42	8703		F	M		150	C	VC		32.46	
6705 6706		C	Q	33.83 71.39	825 825	C	CO	-120	18.54 31.15	8704 8705		F	M		150 150	C	VC		16.16 39.55	
6707		C	Q	33.32	825	С	VC		14.1	8706		s	М		300	С	vc		40.25	
6801	74.77	С	M	71.27	825	С	co		35.05	8707		F	М		150	С	vc		27.16	
6802	74.73 74.73	C	M	71.95	825 825	C	co	20 11	13.52 9.87	8709 8710		S	M		300 375	C	VC		16.7 26.71	
6803 6804		C	M	72.22	525	C	CO	85	22.1	8711		S	M		375	C			32.89	
6805	75	C	М	72.37	450	C	VC	34	41.92	8712		s	М		225	C	vc		24.89	
6806	74.6	С	M		450	С	VC	200000	41.35	8713		S	М		375	C			35.23	
6807 6808	74.75	C	D	72.7 73.75	150 225	C	CO	14	5.49 1.99	8719 8727		F	M		150 150	C	VC		39.84 39.85	
6809		C	M	71.96	525	C	CO	20	1.78	8803		F	G		300	C	VC		131.73	
6810		C	M	73.1	300	С	vc	22	8.74	8901		С	Н	75.17	180	С	PE	151	104.17	
6901		C	M	72.87	450	C	VC		86.8	9501	93.76	C	M	90.29	300	C	VC	21	33.92	
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6904	. 0.05	S	M	74.08	300	C	50	201	19.23	9603		F	м		150	С	vc		33.94	
6905		s	F							9604		F	M						24.04	
7500		F	J		400		110		4.00	9605		F	M						24.9	
7501 7502		F	D		150 150	C	VC		4.68	9606 9607		S	M						31.75 27.13	
7502		F	D		150	c	VC		19.8	9608		S	M						36.32	
7504		s	D		150	С	vc		20	9609		S	M						58.68	
7505		S	D		150	C	VC		25.89	9610		S	M						33.89 25.63	
7506 7507		F	D		150 150	C	vc		26.31 11.14	9611 9612		S	M						32.72	
7508		F	D		150	c	VC		11.34	9613		s	М						17.65	
7509		s	D		150	С	VC		13.89	9701		F	М		150	С	VC		37.65	
7510		F	D		150	C	VC		14.07	9702		S	M		150	С	VC		40.18	
7511 7512		S	D		150 150	C	VC		12.26 12.37	9703 9704		F	M						34.59 34.5	
7513		S	D		150	c	VC		58.66	9707		F	М						31.79	
7514		F	D		150	С	VC		59.25	9708		s	M						35.26	
7515		C	M		100	C	VC		26.73	9709		S	M						24.26	
7516 7517		S	D		150 150	C	VC		17.97 18.21	9710 9711		S	M						52.62 20.98	
7518		S	D		150	c	VC		15.86	9711		F	M						52.41	
7519		F	D		150	С	vc		16.47	9713		F	M						24.44	
7520		S	D		150	C	VC		27.52	9714		S	M						27.33	
April 100		F	D		150	C	VC		27.61	9801		S	M						43.44	
7521 7522		s	D		150	C	VC		14.47	9802		F	M						41.94	

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Princess Avenue, Clitheroe Flood Map (NTH6802S)

Junction

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BBI

SD 74600 42300 National Grid Reference:



North West Region - North Area

Walton Summit, Bamber Bridge. Preston. PR5 8BX Lutra House, Dodd Way, Off Seedlee Road

Tel: 03708 506 506 | www.environment-agency.gov.uk

Map produced on:

Produced by Flood Risk Mapping

6 February 2013

Legend

Modelled Flood Group

Node Point

EA01210PIML01 0471A

Ground

Main River

Flood Zone 3

Flood Zone 2

EA01210PIML01 0392

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will use reasonable care to ensure an accurate copy of the data. The accompanying disclaimer should be used in The datasets used in this plan may not have been audited The Agency cannot ensure that the data in its possession will always be accurate, up to date or valid but the Agency conjunction with this plan

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Flood Zone 2: Shows the additional extent of an extreme flood from rivers to a 0.1% (1 in 1000) chance of Flood Zone 3: Shows the area that could be affected by flooding from rivers or the sea, if there were no defences. This area could be flooded: - or from a river by a flood that has a 1% (1 in 100) chance or greater of happening each year. - from the sea by a flood that has a 0.5% (1 in 200) chance or greater of happening each year.

or the sea, if there were no defences. These outlying areas are likely to be affected by a major flood, that has up occurring each year.

Historic Flooding: We do not hold any records of flooding at this location.

Undefended Level (mAOD)and Flow (m3/sec) data for Clitheroe

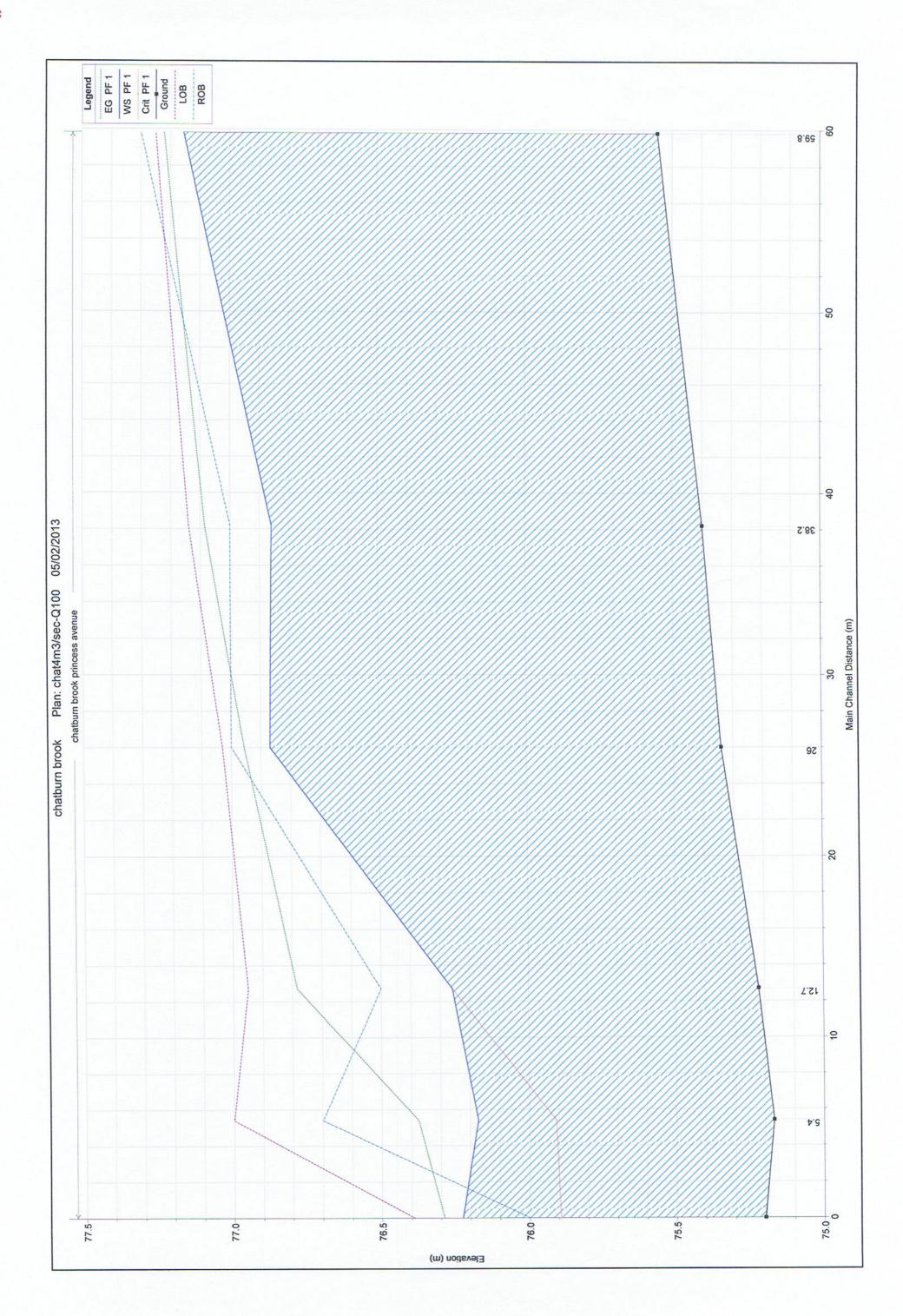
		5	10)	25	2	20)	75	5	100	0	200	0	1000	00
	Level	Flow														
EA01210PIML01_0392	75.45	1.98	75.5	2.27	75.58	2.77	75.67	3.35	75.73	3.77	75.77	4.06	76.03	4.8	77.74	7.66
EA01210PIML01_0421	75.8	1.98	75.85	2.28	75.93	2.77	76.02	3.36	76.07	3.78	76.11	4.07	76.2	4.82	77.74	7.7.7
EA01210PIML01_0461	76.41	1.98	76.47	2.28	76.56	2.78	99.92	3.36	76.72	3.78	92.92	4.08	76.86	4.84	77.75	7.82
EA01210PIML01_0471A	76.52	1.98	76.59	2.28	76.72	2.78	76.87	3.37	76.98	3.79	77.05	4.08	77.23	4.84	77.85	7.82
EA01210PIML01_0471B	76.46	1.98	76.53	2.28	76.63	2.78	76.74	3.37	76.81	3.79	76.85	4.08	96.92	4.84	77.74	7.82

Data taken from Mearley SFRM Study

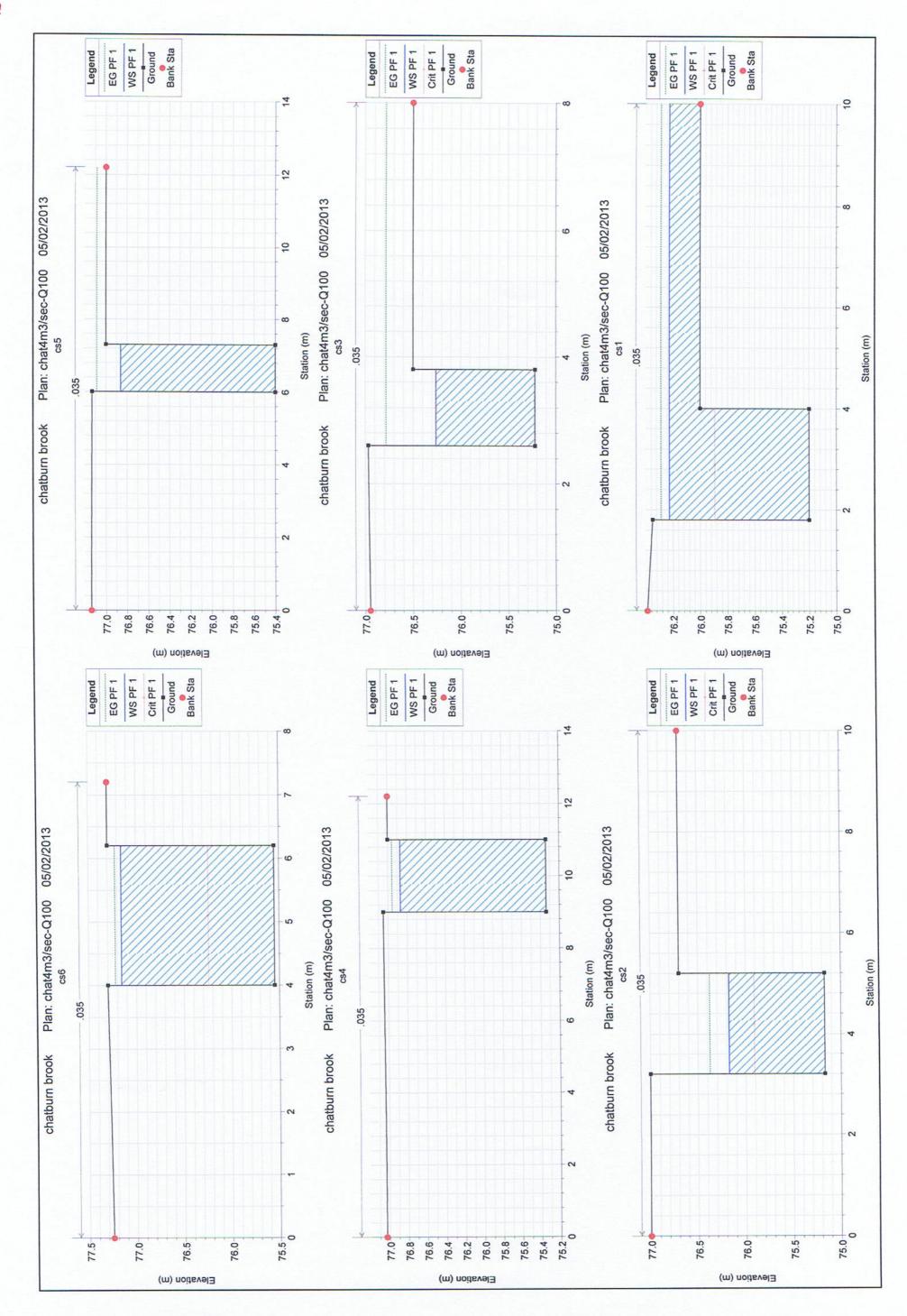
Defended Level (mAOD)and Flow (m3/sec) data for Clitheroe

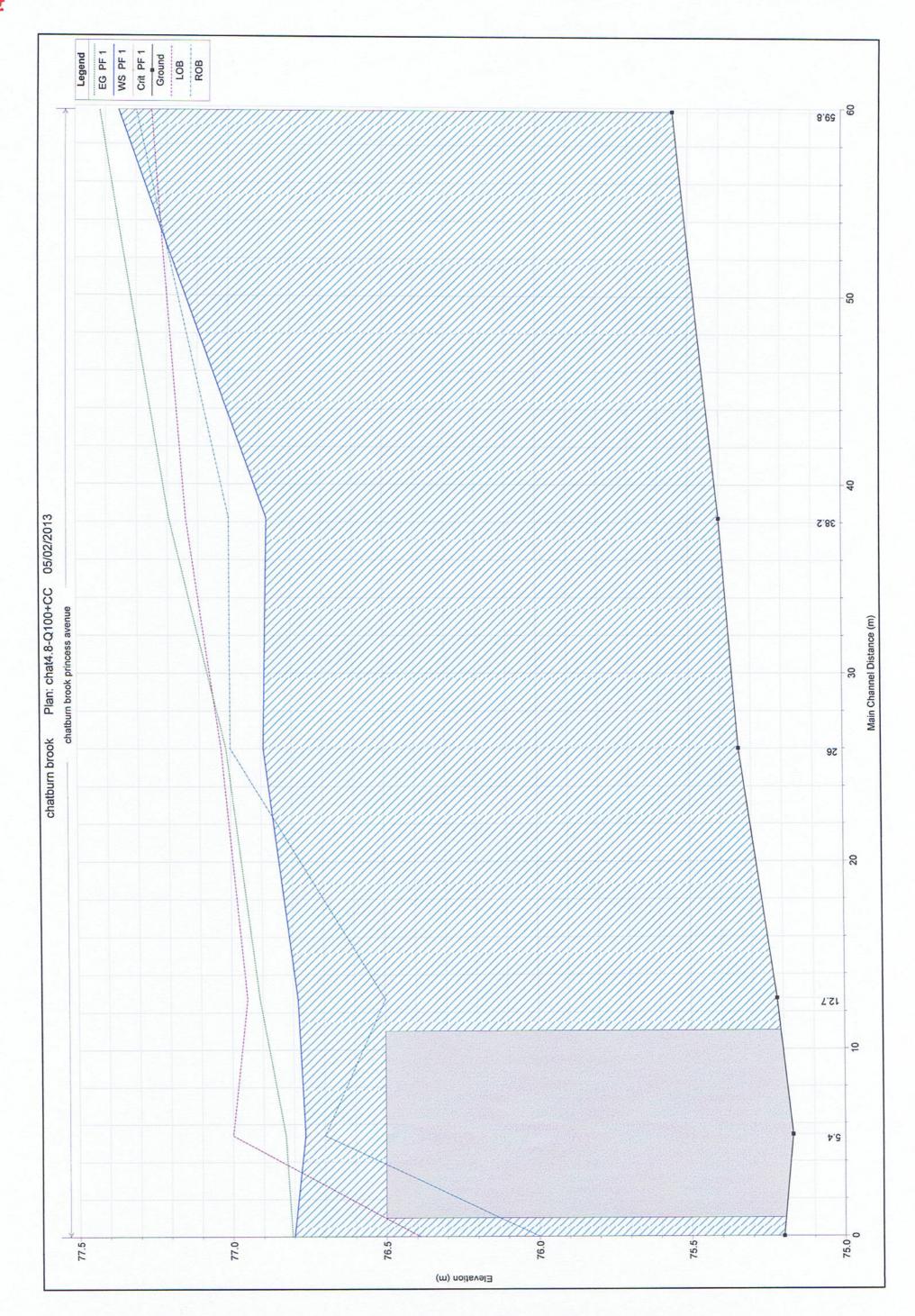
	10	0	S	50	7	75	10	100
	Level	Flow	Level	Flow	Level	Flow	Level	Flow
EA01210PIML01_0392	75.5	0	75.67	0	75.73	3.76	75.77	0
EA01210PIML01_0421	75.85	0	76.02	0	76.07	3.78	76.11	0
EA01210PIML01_0461	76.47	0	99'92	0	76.72	3.78	92'92	0
EA01210PIML01_0471A	76.59	0	76.87	0	76.98	3.78	77.05	0
EA01210PIML01_0471B	76.53	0	76.74	0	76.81	3.78	76.85	0

Data taken from Mearley SFRM Study

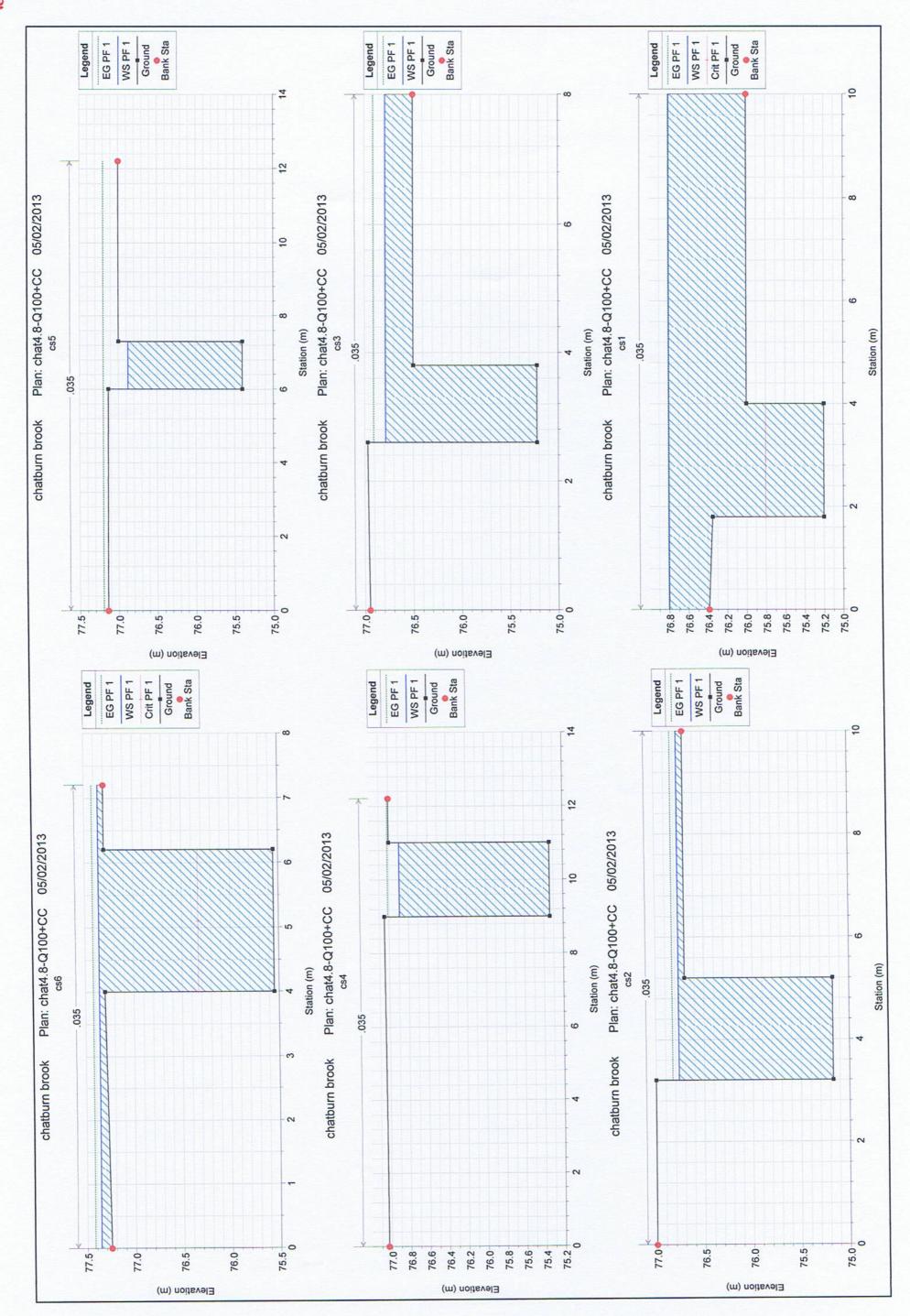


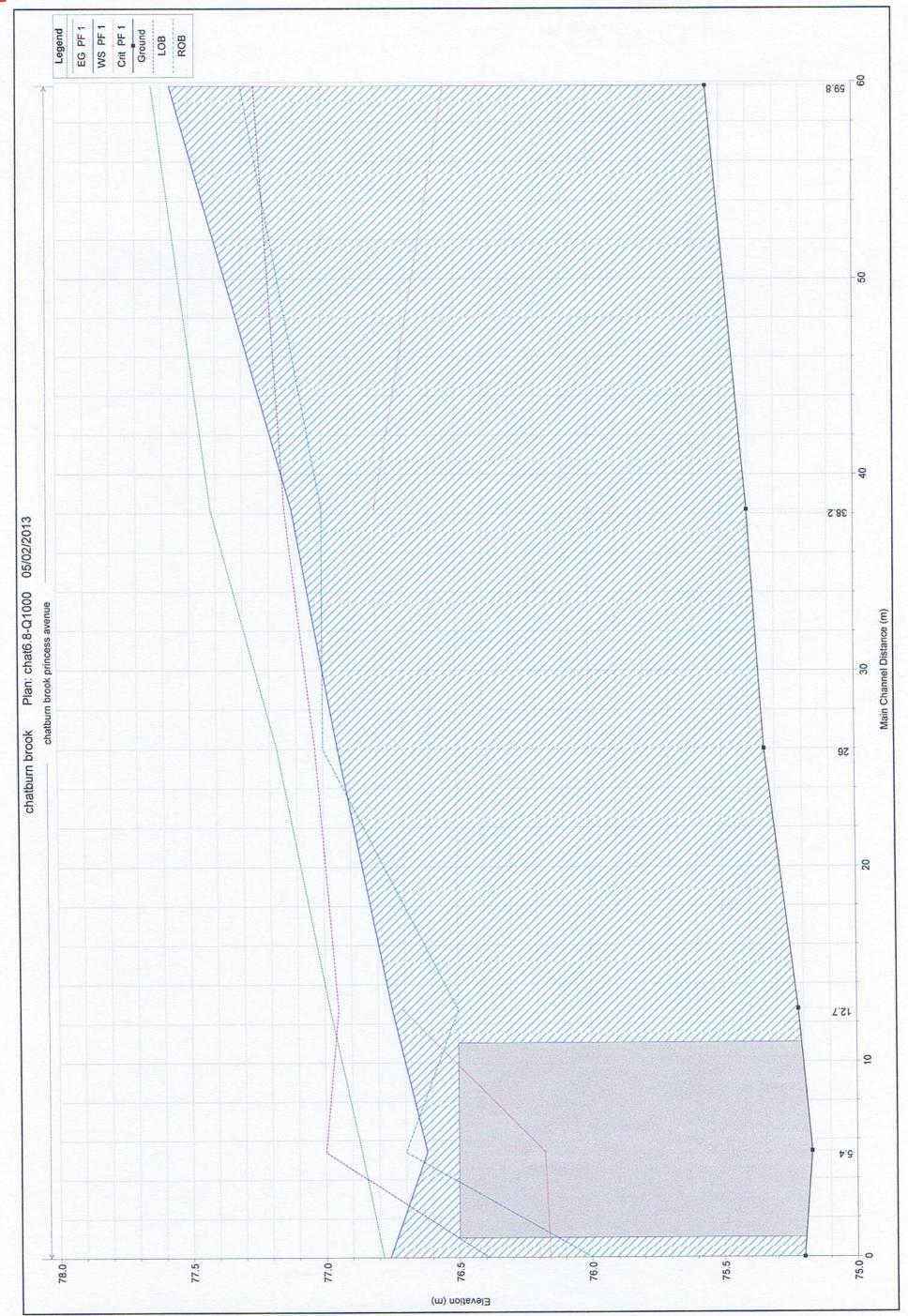
Reach River Sta Profile Q Total Min Ch El W.S.	River Sta	Profile	Q Total	Min Ch El	W.S. Elev	Crit W.S.	E.G. Elev	E.G. Slope	5	Flow Area	Top Width	Fronde # Chl
			(m3/s)	(m)	(m)	(m)	(m)	(m/m)	(s/m)	(m2)	(m)	
orincess avenue	59.8	PF 1	4.00			76.24	77.22	0.002772		3.53	2.20	0.28
princess avenue	38.2	PF 1 5	4.00	75.40			77.09	0.015792		1.90	1.30	0.56
princess avenue	26	PF 1	4.00	75.34	76.87		76.96	0.004098	1.31	3.06	2.00	0.34
princess avenue	12.7	PF 1 3	4.00			76.26	76.78	0.045777		1.25	1.20	1.00
princess avenue	5.4	PF 1		75.17		75.91	76.38	0.012237		2.01	2.00	0.64
princess avenue	0	PF 1	4.00	75.20	76.23	75.89	76.29	0.006000	1.11	3.62	8.20	0.53



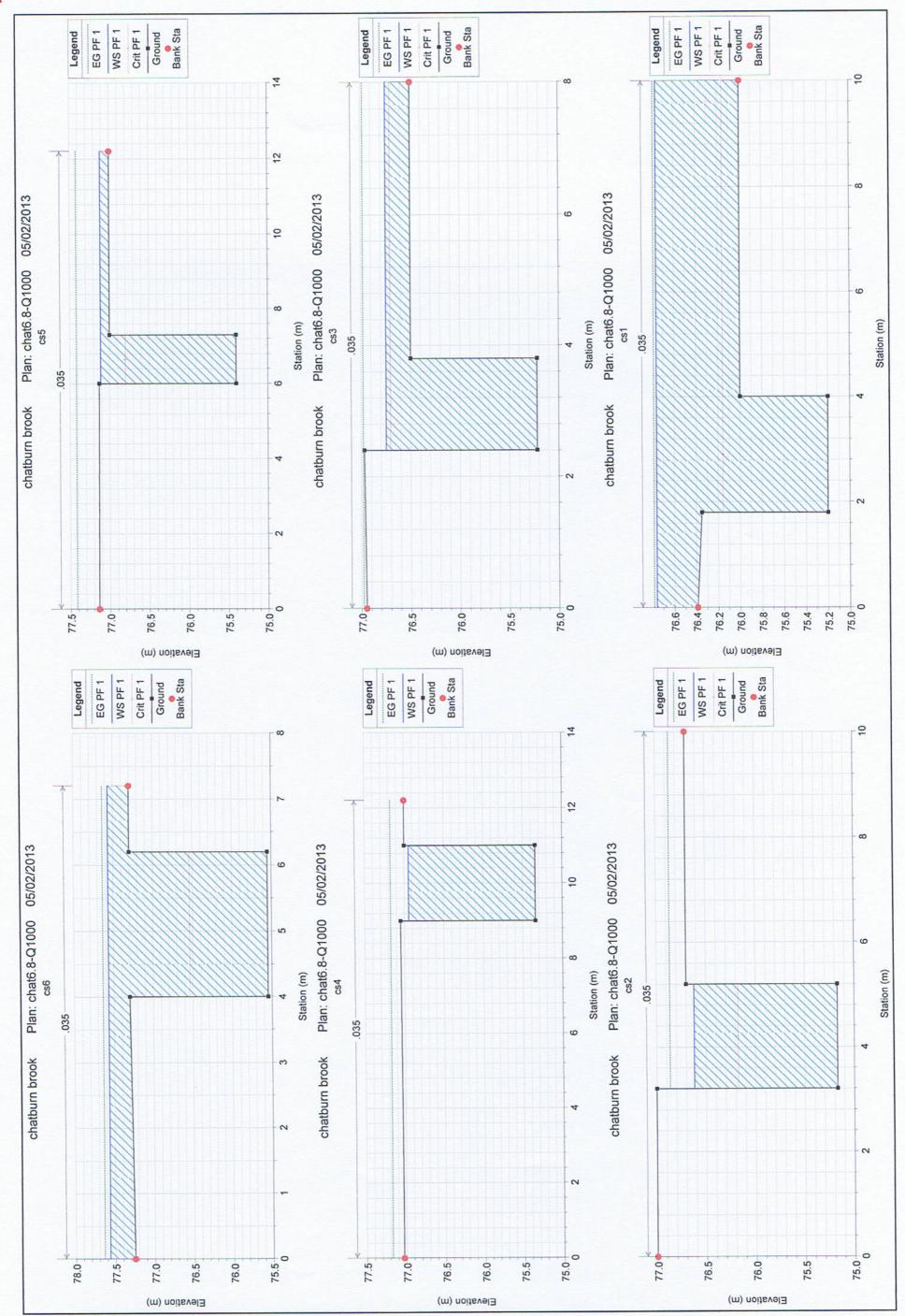


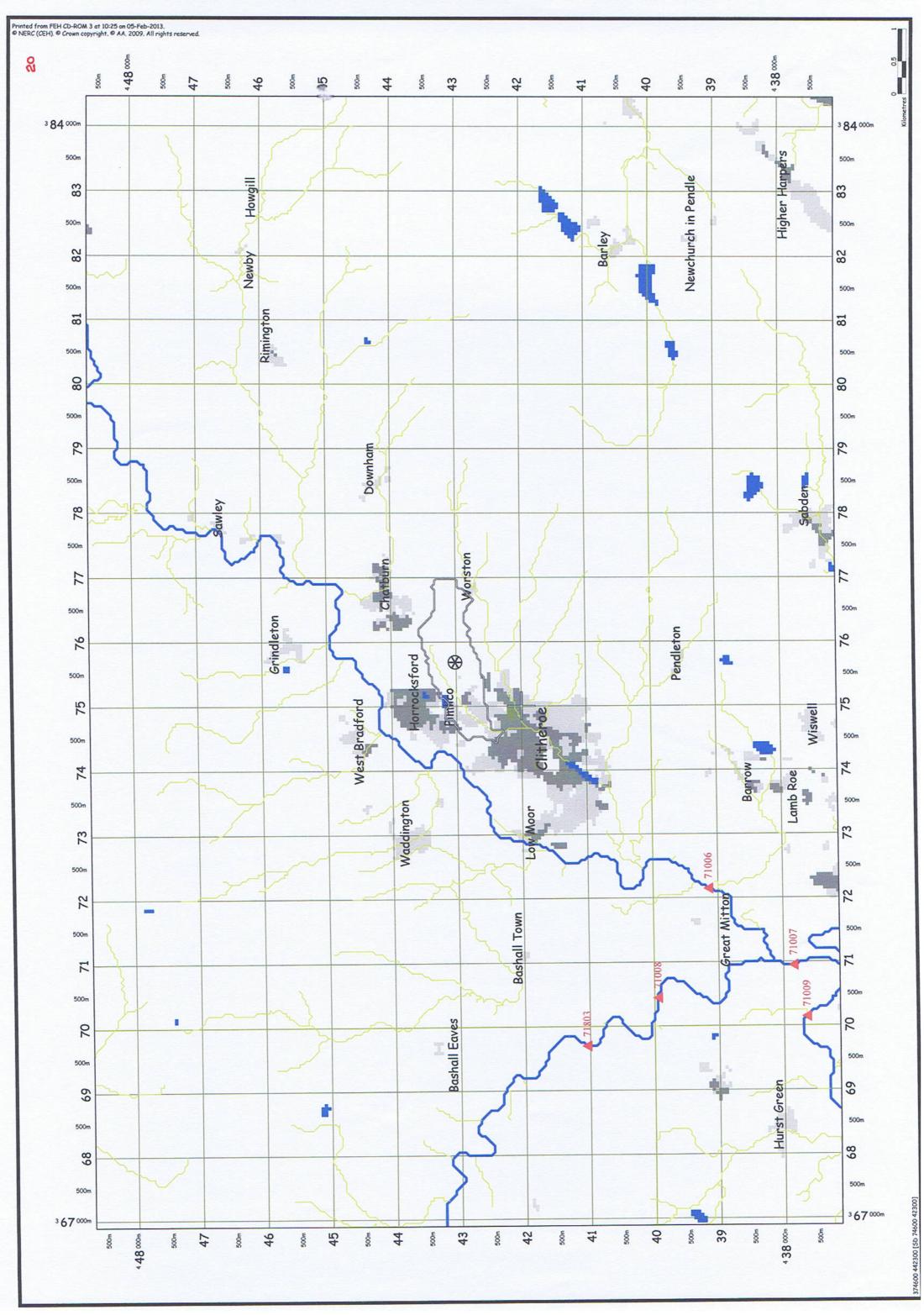
W.S. Elev Crit W.S. E.G. Elev E.G. Slope Vel Chirl Flow Area 1 op Wudth Provided (m) (m) (m/m) (m/m) (m/s) (m2) (m) 77.36 77.42 0.005001 1.10 4.36 7.20 76.88 77.20 0.022100 2.50 1.92 1.30 76.89 77.01 0.005682 1.55 3.10 2.00 76.79 76.79 0.011611 1.56 3.08 5.40 76.76 76.80 76.81 0.006302 1.13 3.49 6.80 76.80 75.80 76.81 0.000253 0.36 9.10 10.00	2 - 101 - 25				TECTION I Iam. DOS INVOIT GRADUIT BLOCK TOOLS								1
59.8 PF 1 4.80 75.55 77.36 76.33 77.42 0.005001 1.10 4.36 7.20 26 PF 1 4.80 75.40 76.89 77.01 0.005682 1.55 3.10 2.00 26 PF 1 4.80 75.22 76.89 77.01 0.005682 1.55 3.10 2.00 12.7 PF 1 4.80 75.22 76.79 76.91 0.011611 1.56 3.08 5.40 11 Lat Struct 76.76 76.83 76.81 76.83 0.006302 1.13 3.49 6.80 5.4 PF 1 3.24 75.80 75.80 76.81 0.000253 0.36 9.10 10.00	Reach	River Sta	Profile	O Total	Min Ch El		Crit W.S.	E.G. Elev	E.G. Slope	>	Flow Area	l op wiath	Fronge # Cui
59.8 PF 1 4.80 75.55 77.36 76.33 77.42 0.005001 1.10 4.36 7.20 38.2 PF 1 4.80 75.40 76.89 77.01 0.005682 1.55 3.10 2.00 26 PF 1 4.80 75.22 76.79 76.91 0.011611 1.56 3.08 5.40 12.7 PF 1 4.80 75.22 76.79 76.91 0.011611 1.56 3.08 5.40 11 Lat Struct 76.76 76.83 76.83 76.83 76.83 76.81 0.006302 1.13 3.49 6.80 6.4 PF 1 3.23 75.20 76.80 76.81 76.81 0.000253 0.36 9.10 10.00	2000	200		(m3/s)	(m)	(m)	(m)	(m)	(m/m)		(m2)	(m)	
38.2 PF 1 4.80 75.40 76.89 77.20 0.0022100 2.50 1.92 1.30 26 PF 1 4.80 75.34 76.89 77.01 0.005682 1.55 3.10 2.00 12.7 PF 1 4.80 75.22 76.79 76.91 0.011611 1.56 3.08 5.40 11 Lat Struct 76.76 76.83 76.83 76.83 76.81 76.81 0.006302 1.13 3.49 6.80 0 PF 1 3.23 75.20 76.80 75.81 76.81 0.000253 0.36 9.10 10.00		0		(6000)			76.33	77.42	0.005001		4.36	7.20	0.45
38.2 PF 1 4.80 75.40 76.88 77.20 0.022100 2.50 1.92 1.30 26 PF 1 4.80 75.34 76.89 77.01 0.005682 1.55 3.10 2.00 12.7 PF 1 4.80 75.22 76.79 76.91 0.011611 1.56 3.08 5.40 11 Lat Struct 76.76 76.83 0.006302 1.13 3.49 6.80 5.4 PF 1 3.24 75.17 76.80 75.81 0.000253 0.36 9.10 10.00	incess avenue	29.8	-	4.60			200						000
26 PF 1 4.80 75.34 76.79 77.01 0.005682 1.55 3.10 2.00 12.7 PF 1 4.80 75.22 76.79 76.91 0.011611 1.56 3.08 5.40 11 Lat Struct 76.76 76.83 0.006302 1.13 3.49 6.80 5.4 PF 1 3.23 75.20 76.80 75.81 0.000253 0.36 9.10 10.00	orinous second	28.2	DE 1	4 80		76.88		77.20	0.022100		1.92	1.30	0.00
26 PF 1 4.80 75.34 76.89 77.01 0.003862 1.35 3.18 5.40 12.7 PF 1 4.80 75.22 76.79 76.91 0.011611 1.56 3.08 5.40 11 Lat Struct 76.76 76.83 0.006302 1.13 3.49 6.80 5.4 PF 1 3.23 75.20 76.80 75.81 0.000253 0.36 9.10 10.00	IIICess aveilue	20.6		2				1000	000000		3 10	200	0.40
12.7 PF 1 4.80 75.22 76.79 76.91 0.011611 1.56 3.08 5.40 7.00 1.27 PF 1 3.94 75.17 76.76 76.81 0.000253 0.36 9.10 10.00 10.00	olineye asooni	26	DF 1	4.80		76.89		10.7/	7990000		2.0	20.4	0
12.7 PF 1 4.80 75.22 76.79 76.91 0.011611 1.30 3.00 3.40 1.40 1.40 1.40 1.40 1.40 1.40 1.40 1	III cass aveilue	20						1			00 6	6 40	0.66
11 Lat Struct 76.76 76.83 0.006302 1.13 3.49 6.80 5.4 PF 1 3.24 75.20 76.80 75.80 76.81 0.000253 0.36 9.10 10.00	incess avenue	12.7	PF 1	4.80		16.79		76.91	0.011611		2.00	0.40	8
11 Lat Struct 5.4 PF 1 3.94 75.17 76.76 76.83 0.006302 1.13 3.49 6.80 0.00 PF 1 3.23 75.20 76.80 75.80 76.81 0.000253 0.36 9.10 10.00				1010101			The latest and the						
5.4 PF 1 3.24 75.17 76.76 76.83 0.006302 1.13 3.49 0.80	incess avenue	11		Lat Struct					11111111	4		000	000
0.37 PF 1 3.23 75.20 76.80 75.80 76.81 0.000253 0.36 9.10 10.00	dinave especie	5.4	PF 1	3.94		76.76		76.83	0.006302	1.13	3.49	0.80	00.0
75.20 76.80 75.80 (1.000233 0.30 0.30	Ilicess aveille	1.5				ľ	11.00	70 04	0 000052	0.36	010	10 00	0.12
	ornave associa		PF 1	3.23			08.67	10.01	0.000233	00.0	9	0	;





W.S. Elev Crit W.S. E.G. Elev E.G. Slope Vel Chil Flow Area 1 op Width (m) (m) (m/m) (m/m) (m/s) (m2) (m) 77.57 76.54 77.64 0.003920 1.16 5.87 7.20 77.11 76.80 77.42 0.038274 2.44 2.78 6.20 76.95 77.17 0.010484 2.12 3.21 2.00 76.75 76.71 76.98 0.021258 2.14 3.18 5.60 76.62 76.18 76.86 0.011850 2.19 2.90 2.00 76.76 76.16 76.78 0.001000 0.69 8.70 10.00	ייייי לכן ייייי לכן יייייי לכן ייייייי לכן יייייייייי				-								
59.8 PF 1 (6.80) 77.57 76.54 77.42 0.003920 1.16 5.87 7.20 26 PF 1 6.80 75.40 77.11 76.80 77.42 0.038274 2.44 2.78 6.20 26 PF 1 6.80 75.40 77.11 76.95 77.17 0.010484 2.12 3.21 2.00 12.7 PF 1 6.80 75.34 76.75 76.77 76.98 0.021258 2.14 3.18 5.60 11. Lat Struct 76.75 76.78 76.18 76.86 0.011850 2.19 2.90 2.00 5.4 PF 1 6.36 75.17 76.76 76.78 0.001000 0.69 8.70 10.00	Reach	River Sta	Profile	O Total	Min Ch El	_	Crit W.S.	E.G. Elev	E.G. Slope		Flow Area	l op Wiath	Fronge # Cui
59.8 PF 1 6.80 75.55 77.57 76.54 77.64 0.003920 1.16 5.87 7.20 38.2 PF 1 6.80 75.40 77.11 76.80 77.42 0.038274 2.44 2.78 6.20 26 PF 1 6.80 75.34 76.95 77.17 0.010484 2.12 3.21 2.00 12.7 PF 1 6.80 75.22 76.75 76.71 76.98 0.021258 2.14 3.18 5.60 11 Lat Struct 76.75 76.78 76.18 76.86 0.011850 2.19 2.90 2.00 5.4 PF 1 6.36 75.17 76.76 76.78 0.001000 0.69 8.70 10.00	1000			(m3/s)	(m)	(m)	(m)	(m)	(m/m)		(m2)	(m)	
38.2 PF 1 6.80 75.40 77.11 76.80 77.42 0.038274 2.44 2.78 6.20 26 PF 1 6.80 75.34 76.95 77.17 0.010484 2.12 3.21 2.00 12.7 PF 1 6.80 75.22 76.75 76.71 76.98 0.021258 2.14 3.18 5.60 11 Lat Struct 75.27 76.78 76.18 76.86 0.011850 2.19 2.90 2.00 5.4 PF 1 6.36 75.27 76.76 76.18 76.78 0.001000 0.69 8.70 10.00		0 0	05.4	6 80			76.54	77.64	0.003920			7.20	0.41
26 PF1 6.80 75.34 76.95 77.17 0.010484 2.12 3.21 2.00 2.00 12.7 PF1 6.80 75.32 76.75 76.71 76.98 0.021258 2.14 3.18 5.60 11. Lat Struct 6.36 75.17 76.62 76.18 76.86 0.011850 2.19 2.90 2.00 0.00 0.00 0.00 8.70 10.00	ncess avenue	0.00		00.0			76.80	77.42	0.038274			6.20	1.16
26 PF 1 6.80 75.22 76.75 76.71 76.98 0.021258 2.14 3.18 5.60 75.02 12.7	ncess avenue	38.2	- 1	00.00	75.24			77 17	0.010484			2.00	0.53
12.7 PF 1 6.80 75.22 76.75 76.71 76.98 0.021258 2.14 3.18 5.50 11 Lat Struct 6.36 75.17 76.62 76.18 76.86 0.011850 2.19 2.90 2.00 12.7 PF 1 6.36 75.17 76.62 76.18 76.78 0.001000 0.69 8.70 10.00	ncess avenue	97	-	0.00	5.0.							00 1	700
11 Lat Struct 5.4 PF 1 6.36 75.17 76.62 76.18 76.86 0.011850 2.19 2.90 2.00 75.20 76.76 76.76 76.78 0.001000 0.69 8.70 10.00	ncess avenue	12.7	PF 1	6.80	75.22		76.71	76.98	0.021258			9.60	16.0
5.4 PF 1 6.36 75.17 76.62 76.18 76.86 0.011850 2.19 2.90 2.00 75.00 PF 1 5.99 75.20 76.76 76.76 76.78 0.001000 0.69 8.70 10.00	ncess avenue	11		Lat Struct									
0.00 pp 1 5.99 75.20 76.76 76.16 76.78 0.001000 0.69 8.70 10.00	olidaye agan	5.4	DF 1	6.36			76.18		0.011850	2.19		2.00	0.58
	moess avenue		DE 1	5 99			76.16		0.001000	69.0		10.00	0.24





VERSION	FEH CD-R	Version	3	exported at	10:25:13	GMT	Tue	05-Feb-13
CATCHMENT	GB	374600		SD 74600 42				
CENTROID	GB	375684		SD 75684 43			1000	-
AREA	1.61			02 1000 1				
ALTBAR	98							
ASPBAR	284						-	
ASPVAR	0.37							
BFIHOST	0.435							
DPLBAR	1.81							
DPSBAR								
	40.3							
FARL	0.995							
FPEXT	0.1073							
FPDBAR	0.798							
FPLOC	0.879							
LDP	3.28							
PROPWET	0.6							
RMED-1H	10.4							
RMED-1D	42.4							
RMED-2D	58.8						E TRAINE	
SAAR	1222							
SAAR4170	1159							
SPRHOST	30.24							
URBCONC1990	0.325							
URBEXT1990	0.035							
URBLOC1990	0.455							
URBCONC2000	0.455							
URBEXT2000								
	0.098							
URBLOC2000	0.441							
С	-0.02592							
D1	0.41741							
D2	0.38874							
D3	0.43324		4					
E	0.30185							
F	2.45601							
C(1 km)	-0.025							
D1(1 km)	0.405							
D2(1 km)	0.385							
D3(1 km)	0.437							
E(1 km)	0.301							
F(1 km)	2.458							
. ()								
	-							
Michael Lamber	t Associates			Copyright un	der licence	from IoH		
Catchment descri	iptors							
	Princess Av	onuo		05/02/2013	mal			B1343

	FEH CD-R	version	3	exported at			Tue	05-Feb-13			B1343
Parameters		r-11			Clitheroe rai						
	Design rain				06/02/2013	mel					
	Typical poir			440000	00 74000 4	0000					
Catchment	Catchment	GB	374600	442300	SD 74600 4	2300					
			km**2								
Ouration=	6	1	(hours)								
ixed durat											
Return peri		1	(years)					TO VALUE OF			
Annual max				14 11 2							
;	d1	d2	d3	e	f		The same of				
-0.02592		0.38874		0.30185	2.45601						
n areal re	duction factor	or of 0.976 h	nas been ap	plied to a po	int rainfall of	79.7 mm to	yield a catc	hment desig	n rainfall of	77.8 mm.	
lo warning	(s) or note(s	s) were pres	ent for this o	alculation.							
					sliding duration	ons.					
			10	20			200	500			
Ouration	Duration	Duration			year rainfall						
ninutes	hours	days	mm	mm	mm	mm	mm	mm			-
15	0.25		12.89	16.44	22.52	28.51	36.06	49.16			
30	0.5		16.85								
45	0.75	0.020633		21.21	28.57	35.72	44.62	59.84			
60			19.66	24.57	32.77	40.67	50.44	66.99			
	1 25		21.92	27.24	36.09	44.56	54.97	72.52			
75	1.25	0.052083	23.84	29.51	38.88	47.81	58.74	77.09			
90	1.5	0.0625	25.53	31.49	41.31	50.63	62	81.01			
105	1.75		27.05	33.26	43.47	53.13	64.89	84.47			
120	2	0.083333	28.43	34.88	45.44	55.4	67.49	87.58			
135	2.25	0.09375	29.71	36.36	47.24	57.47	69.87	90.41			
150	2.5		30.89	37.74	48.9	59.38	72.06	93.01			
165	2.75	0.114583	32.01	39.03	50.46	61.17	74.1	95.43			
180	3	0.125	33.06	40.25	51.92	62.84	76.01	97.68			
195	3.25		34.05	41.4	53.3	64.42	77.8	99.8			
210	3.5		35	42.49	54.61	65.92	79.5	101.8			
225	3.75	0.15625	35.91	43.53	55.86	67.34	81.11				
240	3.75	0.166667	36.77					103.69			
				44.53	57.05	68.69	82.65	105.5			
255	4.25		37.61	45.49	58.19	69.99	84.12	107.22			
270	4.5	0.1875	38.41	46.41	59.29	71.23	85.53	108.86			
285	4.75		39.18	47.3	60.35	72.43	86.88	110.44			
300	5	0.208333	39.93	48.16	61.36	73.59	88.18	111.96			
315	5.25	0.21875	40.66	48.99	62.35	74.7	89.44	113.43			
330	5.5	0.229167	41.36	49.79	63.3	75.78	90.65	114.84		-	-
345	5.75	0.239583	42.04	50.57	64.22	76.82	91.83	116.2			
360	6	0.25	42.71	51.33	65.12	77.83	92.96	117.52			
375	6.25		43.35	52.07	65.99	78.81	94.07	118.8			
390		0.270833	43.98	52.78	66.84			7 - 7 - 7			
405						79.77	95.14	120.04			
	6.75	0.28125	44.6	53.48	67.66	80.7	96.18	121.25			
420	7 7 7 7		45.2	54.17	68.46	81.6	97.2	122.43			
435	7.25		45.79	54.83	69.25	82.49	98.19	123.57			
450	7.5		46.36	55.49	70.02	83.35	99.15	124.68			
465	7.75		46.92	56.12	70.77	84.19	100.1	125.77			
480	8	0.333333	47.47	56.75	71.5	85.01	101.02	126.83			
495	8.25	0.34375	48.01	57.36	72.22	85.82	101.92	127.87		The same	
510	8.5		48.54	57.96	72.92	86.61	102.8	128.88			
525	8.75	THE RESIDENCE OF THE PARTY OF T	49.06	58.55	73.61	87.38	103.66	129.87			
540	9		49.57	59.13	74.28	88.13	104.5	130.84			
555	9.25	The second secon	50.07	59.69	74.94	88.88	105.33	131.79			
570	9.5		50.56	60.25	The second secon		The second secon			-	-
					75.59	89.6	106.14	132.72			
585	9.75		51.05	60.8	76.23	90.32	106.94	133.64			
600	10	-	51.52	61.34	76.86	91.02	107.72	134.53			
615	10.25			61.86	77.48	91.71	108.49	135.41			
630	10.5		52.45	62.39	78.08	92.39	109.24	136.27			
645	10.75	THE RESERVE AND ADDRESS OF THE PARTY OF THE	52.91	62.9	78.68	93.05	109.98	137.12			
660	11		53.35	63.4	79.27	93.71	110.71	137.96			
675	11.25		53.8	63.9	79.85	94.35	111.43	138.78			
690		0.479167	54.23	64.39	80.42	94.99	112.14	139.58			
705	11.75		54.66	64.87	80.98	95.62	112.83	140.38			
720	12	0.40000	55.08	65.35	81.53	96.23	113.52	141.16			
735	12.25		55.47	65.78							
					82.03	96.78	114.12	141.84			
750	12.5		55.85	66.21	82.52	97.32	114.72	142.51			
765	12.75	The second secon	56.22	66.62	83	97.86	115.31	143.18			
780	13		56.59	67.04	83.48	98.39	115.89	143.83			
795	13.25		56.95	67.45	83.94	98.9	116.46	144.48			
810	13.5	0.5625	57.31	67.85	84.41	99.42	117.02	145.11		Treatment when	
825	13.75	0.572917	57.67	68.25	84.87	99.92	117.58	145.74			
	14	THE RESERVE OF THE PARTY OF THE	58.02	68.64	85.32	100.42	118.13	146.35			